Wind Load Report - Sperling

1. Site & Building Data

Roof Type:	Gable
Wind Speed (ult):	170 mph
Exposure Category:	C
Enclosure Class:	Enclosed
Building Width (W):	50 ft.
Building Length (L):	50 ft.
Eave Height (h_e):	10 ft.
Foundation Height (h_f):	0 ft.
Roof Pitch:	4 /12
Eave Overhang (OH_e):	2 ft.
Gable Overhang (OH_g):	1 ft.

2. Parameters & Coefficients

Topographic Factor (K_{zt}):	1.0
Directionality Factor (K_d):	.85
Roof Angle (θ):	18.43 deg.
Mean Roof Height (h):	14.17 ft.
Ridge Height (h_r):	18.33 ft.
Pos. Internal Pressure (+GCpi):	+0.18
Neg. Internal Pressure (-GCpi):	-0.18
Velocity Pressure Exp. Coeff. (K_h):	0.85 @ z=h
Velocity Pressure (q_h):	53.38 psf
End Zone Width (a):	3.00 ft.
Zone 2/2E Dist.:	25.00 ft.

3. Design Assumptions and Notes

Code Standard:	ASCE 7-10
Geometry:	Regular-Shaped Bldg.
Height Class:	Low-Rise Building
Notes:	

4. Design Loads

Top Chord Dead Load:	7 psf
Bottom Chord Dead Load:	10 psf
Truss/Rafter Spacing:	24 in. o/c

4. Design Wind Pressures: MWFRS Envelope Procedure

Load Case A: Transverse Direction

Surface	GCpf	Design Pressure (psf)	
		(w/ +GCpi)	(w/ -GCpi)
1	0.52	17.96	37.18
2	-0.69	-46.44	-27.23
3	-0.47	-34.62	-15.40
4	-0.42	-31.78	-12.57
1E	0.78	32.04	51.26
2E	-1.07	-66.73	-47.51
3E	-0.67	-45.55	-26.33
4E	-0.62	-42.60	-23.39
2OH	-0.69	-36.83	
2EOH	-1.07	-57.12	
3OH	-0.47	-25.01	
3EOH	-0.67	-35.94	
2OH+W	-0.69/-0.7	-74.20	
2EOH+W	-1.07/-0.7	-94.49	

a) (+) and (-) signs signify wind pressures acting toward & away from surfaces.
b) External Pressure Coefficients linearly interpolated from Fig. 28.4-1 ASCE 7-10.
c) Design building for all wind directions, 4 load patterns per load case.
d) Total horizontal shear shall not be less than that by neglecting roof wind forces.
e) Min. wind load for enclosed or partially enclosed bldg.: 16 psf wall, 8 psf roof.
f) Design pressures are for strength design, multiply by 0.6 for ASD.

Load Case B: Longitudinal Direction

Surface	GCpf	Design Pressure (psf) (w/ +GCpi)	Design Pressure (psf) (w/ -GCpi)
1	-0.45	-33.63	-14.41
2	-0.69	-46.44	-27.23
3	-0.37	-29.36	-10.14
4	-0.45	-33.63	-14.41
5	0.40	11.74	30.96
6	-0.29	-25.09	-5.87
1E	-0.48	-35.23	-16.01
2E	-1.07	-66.73	-47.51
3E	-0.53	-37.90	-18.68
4E	-0.48	-35.23	-16.01
5E	0.61	22.95	42.17
6E	-0.43	-32.56	-13.35
2OH	-0.69	-36.83	
2EOH	-1.07	-57.12	
3OH	-0.37	-19.75	
3EOH	-0.53	-28.29	
2EOH+W	-1.07/-0.7	-94.49	
3EOH+W	-0.53/-0.7	-65.66	

a) (+) and (-) signs signify wind pressures acting toward & away from surfaces.
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Torsional Load Cases

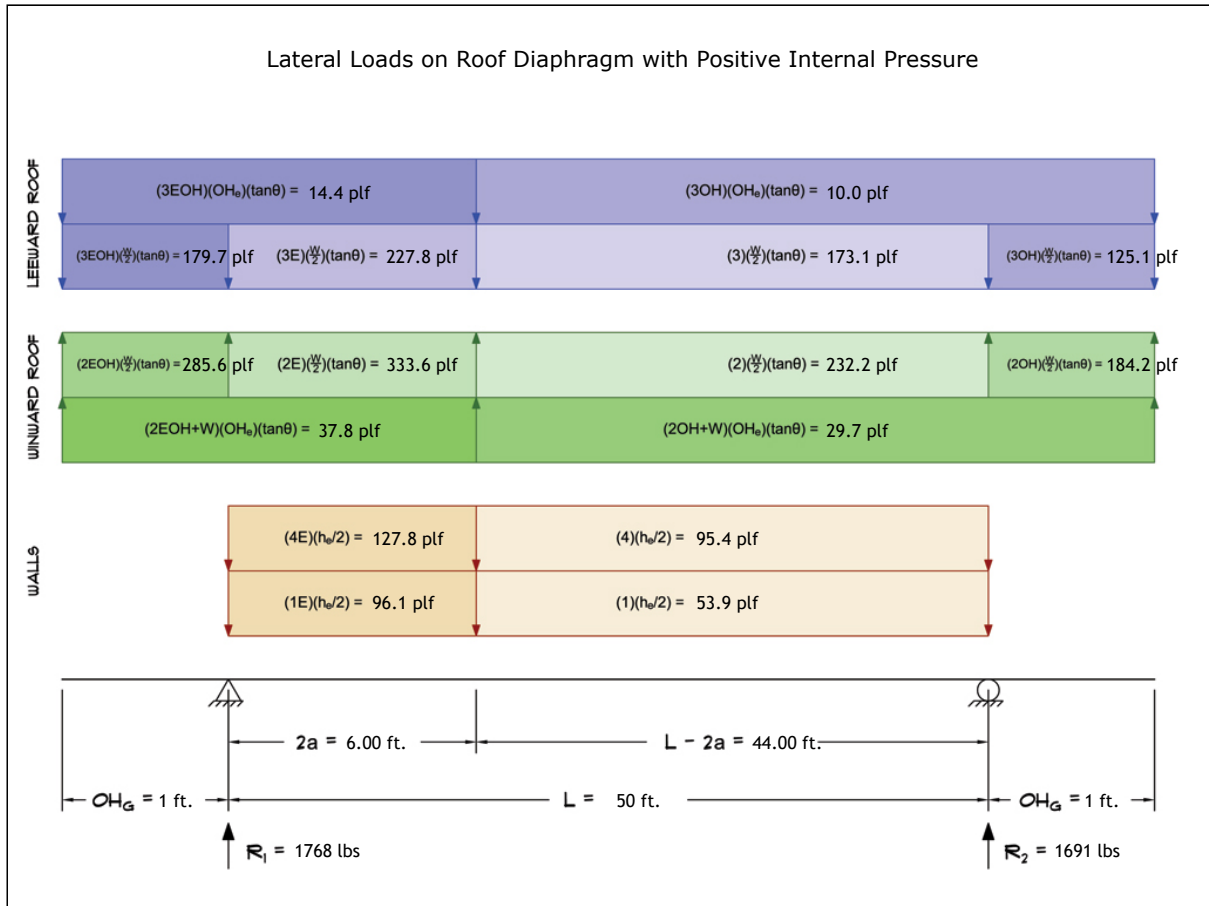| Surface	Load Case	GCpf	Design Pressure (psf) (w/ +GCpi)	Design Pressure (psf) (w/ -GCpi)
1T	A	-	4.49	9.29
2T	A	-	-11.61	-6.81
3T	A	-	-8.66	-3.85
4T	A	-	-7.95	-3.14
5T	B	-	2.94	7.74
6T	B	-	-6.27	-1.47

a) (+) and (-) signs signify wind pressures acting toward & away from surfaces.
b) Pressures designated with a "T" are 25% of full design wind pressures.
c) Torsional loading shall apply to all 8 load patterns using the figures shown.
d) Design pressures are for strength design, multiply by 0.6 for ASD.
e) Torsional Design Exceptions: One story bldg. with h ≤ 30 ft,
   Two stories or less framed with light frame construction,
   Two stories or less with flexible diaphragms.

Case A Torsion — Transverse Direction

Case B Torsion — Longitudinal Direction

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Wind Loads			001

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5. Wind Load Calculations

1.) Lateral Loads - Transverse Direction:

Lateral Loads on Roof Diaphragm with Positive Internal Pressure

LEEWARD ROOF

$(3EOH)(OH_e)(\tan\theta) = 14.4$ plf $\qquad (3OH)(OH_e)(\tan\theta) = 10.0$ plf

$(3EOH)(\frac{W}{2})(\tan\theta) = 179.7$ plf $(3E)(\frac{W}{2})(\tan\theta) = 227.8$ plf $(3)(\frac{W}{2})(\tan\theta) = 173.1$ plf $(3OH)(\frac{W}{2})(\tan\theta) = 125.1$ plf

WINWARD ROOF

$(2EOH)(\frac{W}{2})(\tan\theta) = 285.6$ plf $(2E)(\frac{W}{2})(\tan\theta) = 333.6$ plf $(2)(\frac{W}{2})(\tan\theta) = 232.2$ plf $(2OH)(\frac{W}{2})(\tan\theta) = 184.2$ plf

$(2EOH+W)(OH_e)(\tan\theta) = 37.8$ plf $\qquad (2OH+W)(OH_e)(\tan\theta) = 29.7$ plf

WALLS

$(4E)(h_e/2) = 127.8$ plf $\qquad (4)(h_e/2) = 95.4$ plf

$(1E)(h_e/2) = 96.1$ plf $\qquad (1)(h_e/2) = 53.9$ plf

$2a = 6.00$ ft. $\qquad L - 2a = 44.00$ ft.

$OH_G = 1$ ft. $\qquad L = 50$ ft. $\qquad OH_G = 1$ ft.
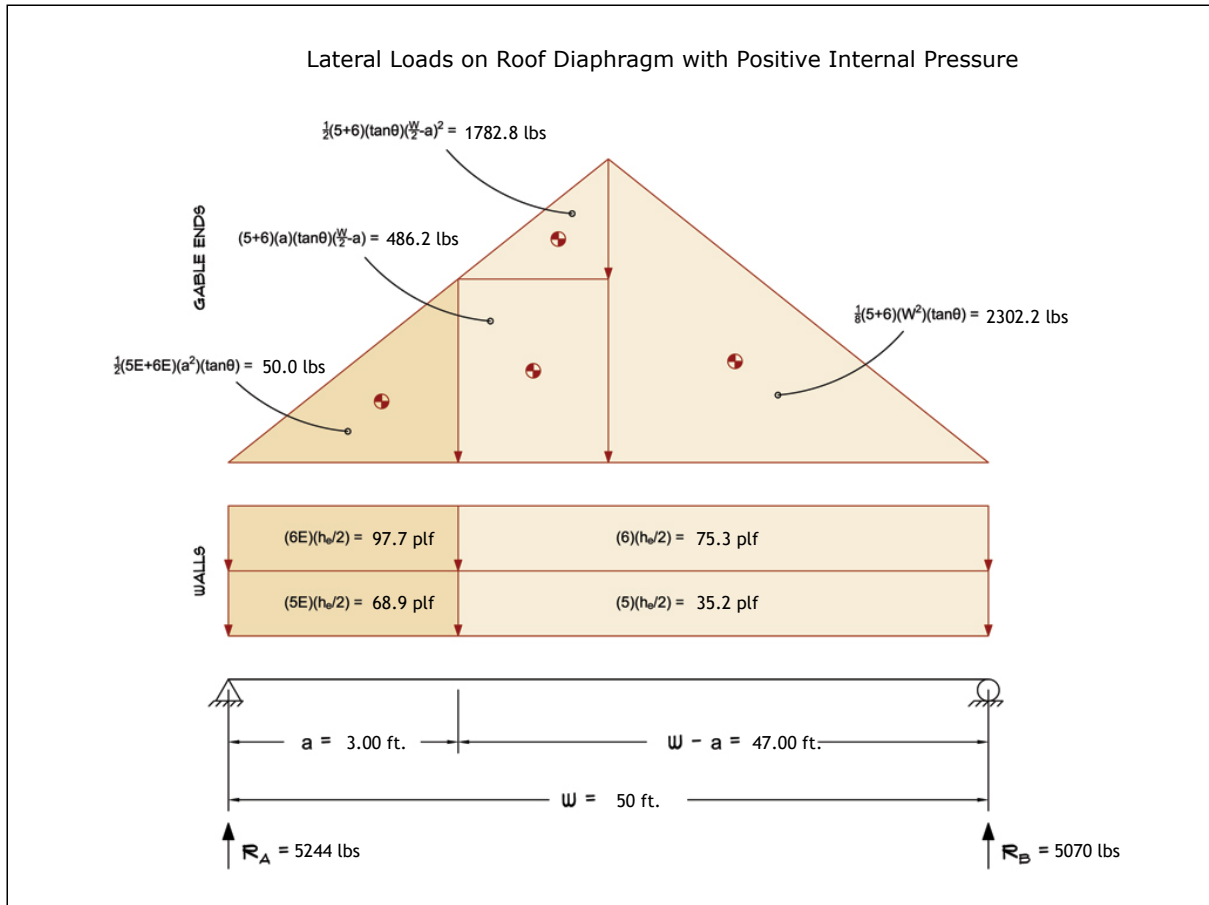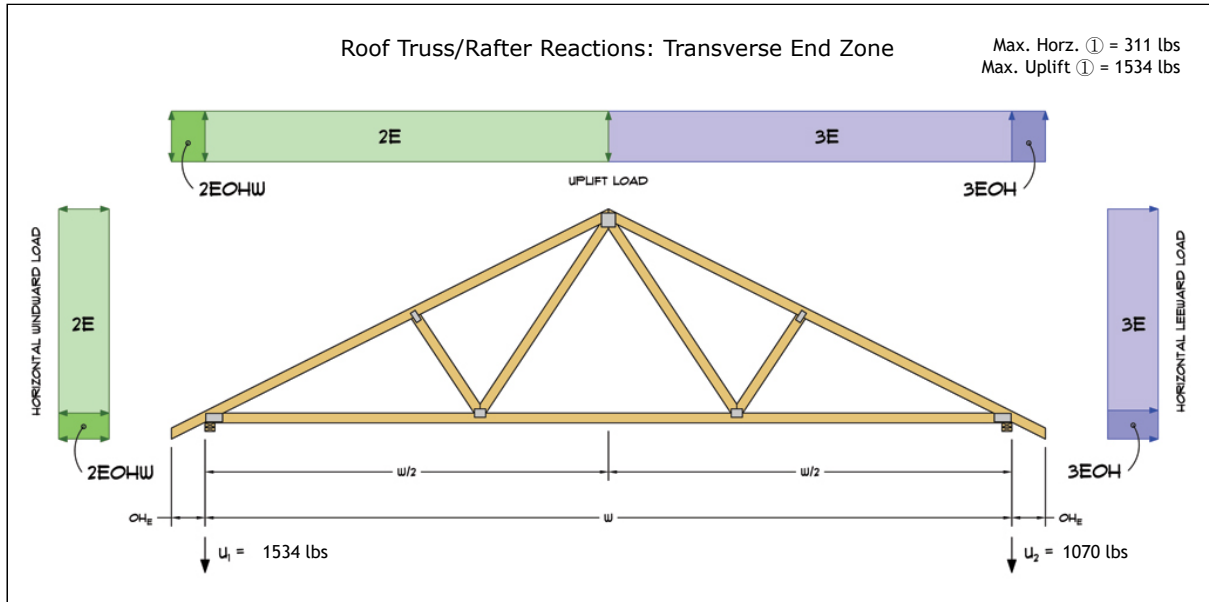
$R_1 = 1768$ lbs $\qquad R_2 = 1691$ lbs

a) (-) signs signify wind lateral forces acting opposite to the direction of the arrows shown.
b) Strength design values multiplied by 0.6 to obtain ASD values.

Wind Base Shear (ASD)						
Load Case A: Transverse Direction						
Load Case	Walls (lbs)	Roof (lbs)	Roof Overhangs (lbs)	Total Lateral Load (lbs)	R_1 (lbs)	R_2 (lbs)
Positive Internal Pressure	7910	-3236	-1214	3459	1768	1691
Negative Internal Pressure	7910	-3236	-1214	3459	1768	1691
Roof Pressure = 0	7910	0	0	7910	4152	3758
Min. Pressures (8 psf, 16 psf)	2400	2000	246	4646	2323	2323

a) Bottom half of wall neglected in tributary area calculations.
b) Strength design values multiplied by 0.6 to obtain ASD values.

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2.) Lateral Loads - Longitudinal Direction:

Lateral Loads on Roof Diaphragm with Positive Internal Pressure

$\frac{1}{2}(5+6)(\tan\theta)(\frac{W}{2}-a)^2 = 1782.8$ lbs

$(5+6)(a)(\tan\theta)(\frac{W}{2}-a) = 486.2$ lbs

$\frac{1}{8}(5+6)(W^2)(\tan\theta) = 2302.2$ lbs

$\frac{1}{2}(5E+6E)(a^2)(\tan\theta) = 50.0$ lbs

GABLE ENDS

$(6E)(h_e/2) = 97.7$ plf

$(6)(h_e/2) = 75.3$ plf

$(5E)(h_e/2) = 68.9$ plf

$(5)(h_e/2) = 35.2$ plf

WALLS

$a = 3.00$ ft.

$W - a = 47.00$ ft.

$W = 50$ ft.

$R_A = 5244$ lbs

$R_B = 5070$ lbs

a) (-) signs signify wind lateral forces acting opposite to the direction of the arrows shown.
b) Strength design values multiplied by 0.6 to obtain ASD values.
c) Where the length of building (L) exceeds 4X the mean roof height (h), wind drag forces should additionally be considered.

Wind Base Shear (ASD)						
Load Case B: Longitudinal Direction						
Load Case	Walls (lbs)	Gable Ends (lbs)	Roof (lbs)	Total Lateral Load (lbs)	R_A (lbs)	R_B (lbs)
Positive Internal Pressure	5693	4621	0	10314	5244	5070
Negative Internal Pressure	5693	4621	0	10314	5244	5070
Roof Pressure = 0	5693	4621	0	10314	5244	5070
Min. Pressures (8 psf, 16 psf)	2400	2000	0	4400	2200	2200

a) Bottom half of wall neglected in tributary area calculations.
b) Strength design values multiplied by 0.6 to obtain ASD values.

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3.) <u>Roof Truss Reactions</u>:

Roof Truss/Rafter Reactions: Transverse End Zone

Max. Horz. ① = 311 lbs
Max. Uplift ① = 1534 lbs

a) Strength design values multiplied by 0.6 to obtain ASD values.
b) Windward loads may be positive or negative depending on pitch of roof.

Roof Truss/Rafter Reactions (ASD)					
w/ Positive Internal Pressure					
Load Case	Horizontal Load (lbs)	Gross Uplift (lbs)	Net Uplift (lbs)	U_1 (lbs)	U_2 (lbs)
Transverse Int. Zone	158	2670	1592	946	646
Transverse End Zone	259	3681	2603	1534	1070
Longitudinal Int. Zone	184	2410	1332	815	516
Longitudinal End Zone	311	3344	2266	1385	881

a) Gross Uplift calculations do not include any counteracting roof dead loads.
b) Net Uplift calculations include counteracting roof dead loads multiplied by 0.6 per load case (7) ASCE 7-10.
c) Strength design values multiplied by 0.6 to obtain ASD values for wind loads.
d) Loads based on truss spacing calculated at 24" o/c.
e) Negative values for horizontal load indicate load acting in windward direction (tranverse load cases).
f) Negative values for uplift indicate net downward force (zero uplift).

*Disclaimer: The calculations produced herein are for initial design and estimating purposes only. The calculations and drawings presented do not constitute a fully engineered design. All of the potential load cases required to fully design an actual structure may not be provided by this calculator. For the design of an actual structure, a registered and licensed professional should be consulted as per IRC 2012 Sec. R802.10.2 and designed according to the minimum requirements of ASCE 7-10. The wind load calculations provided by this online tool are for educational and illustrative purposes only. Medeek Design assumes no liability or loss for any designs presented and does not guarantee fitness for use.