



# Beam Design - THOMPSON ADDITION

## 1. Beam Data

Load Type: Uniform Dist. Load  
 Support: Simple Beam  
 Beam Type: Sawn Lumber  
 Species: Douglas Fir-Larch  
 Grade: DF No.2  
 Size: 4 x 10  
 Design Span (L): 8.75 ft.  
 Clear Span: 8.50 ft.  
 Total Span: 9.00 ft.  
 Bearing (lb): 3 in.  
 Quantity (N): 1

## 2. Design Loads

Live Load: 360 plf  
 Dead Load: 60 plf  
 Selfweight: 69.8 lbs  
 Dist. Selfweight: 7.97 plf  
 Total Weight: 71.8 lbs

## 3. Design Options

Lateral Support: unbraced  
 Defl. Limits: 360|240  
 Load Duration: 1.15  
 Exposure: wet  
 Temperature:  $T \leq 100^{\circ}\text{F}$   
 Orientation: Vertical  
 Incised Lumber: Yes  
 Rep. Members: Yes

## 4. Design Assumptions and Notes

Code Standard: IBC 2015, NDS 2015  
 Bending Stress: Parallel to Grain  
 Notes: BEAM

## 5. Adjustment Factors

Factor	Description	$F_b$	$F_t$	$F_v$	$F_c$	$F_{c\perp}$	$E/E_{min}$
$C_D$	Load Duration Factor	1.15	1.15	1.15	1.15	-	-
$C_M$	Wet Service Factor	$1^b$	1	0.97	$0.8^c$	0.67	0.9
$C_t$	Temperature Factor	1	1	1	1	1	1
$C_L$	Beam Stability Factor	0.981	-	-	-	-	-
$C_F$	Size Factor	1.2	1.1	-	1	-	-
$C_{fu}$	Flat Use Factor	$1.1^d$	-	-	-	-	-
$C_i$	Incising Factor	0.8	0.8	0.8	0.8	1	0.95
$C_r$	Repetitive Member Factor	1.15	-	-	-	-	-

a) Adjustment factors per AWC NDS 2015 and NDS 2015 Supplement.

b) When  $(F_b)(C_F) \leq 1,150$  psi,  $C_M = 1.0$ .

c) When  $(F_c)(C_F) \leq 750$  psi,  $C_M = 1.0$ .

d) Only applies when sawn lumber or glulam beams are loaded in bending about the y-y axis.

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## 6. Beam Calculations

Determine reference design values, sectional properties and self weight of beam:

$$A = b \times d$$

,

,

where:

b = Breadth of rectangular beam in bending (in.)

d = Depth of rectangular beam in bending (in.)

A = Cross sectional area of beam (in.<sup>2</sup>)

S<sub>x</sub> = Section modulus about the X-X axis (in.<sup>3</sup>)

S<sub>y</sub> = Section modulus about the Y-Y axis (in.<sup>3</sup>)

I<sub>x</sub> = Moment of inertia about the X-X axis (in.<sup>4</sup>)

I<sub>y</sub> = Moment of inertia about the Y-Y axis (in.<sup>4</sup>)

$$b = 3.500 \text{ in.}$$

$$d = 9.250 \text{ in.}$$

$$A = 3.500 \times 9.250 = 32.38 \text{ in.}^2$$

$$S_x = (3.500)(9.250)^2/6 = 49.91 \text{ in.}^3$$

$$S_y = (3.500)^2(9.250)/6 = 18.89 \text{ in.}^3$$

$$I_x = (3.500)(9.250)^3/12 = 230.84 \text{ in.}^4$$

$$I_y = (3.500)^3(9.250)/12 = 33.05 \text{ in.}^4$$

Reference Design Values from Table 4A NDS Supplement (Reference Design Values for Visually Graded Dimension Lumber, 2" - 4" thick).

Species & Grade	F <sub>b</sub>	F <sub>t</sub>	F <sub>v</sub>	F <sub>c⊥</sub>	F <sub>c</sub>	E	E <sub>min</sub>	G
DF No.2	900	575	180	625	1350	1600000	580000	0.5

The following formula shall be used to determine the density of wood (lbs/ft<sup>3</sup>). (NDS Supplement Sec. 3.1.3)

where:

ρ<sub>w</sub> = Density of wood (lbs/ft<sup>3</sup>)

G = Specific gravity of wood (dimensionless)

m.c. = Moisture content of wood (percentile)

$$G = 0.5$$

$$\text{m.c.} = 28 \% \text{ (Estimated moisture content at wet service conditions)}$$

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$$= 35.47 \text{ lbs/ft}^3$$

$$\text{Volume}_{\text{total}} = N[A \times (L + l_b)] = 1 \times [32.38 \times (105.00 + 3)] \times (12 \text{ in./ft.})^3 = 2.02 \text{ ft}^3$$

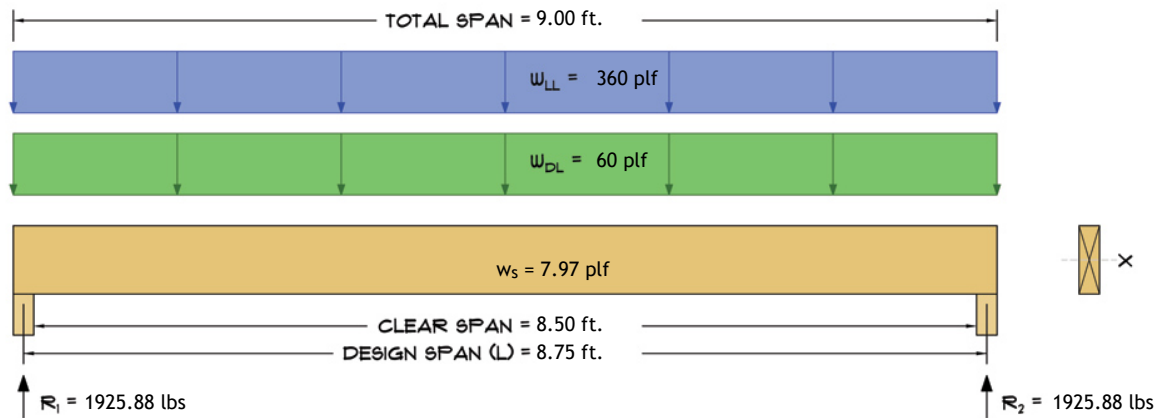
$$\text{Volume}_{\text{span}} = N[A \times L] = 1 \times [32.38 \times 105.00] \times (12 \text{ in./ft.})^3 = 1.97 \text{ ft}^3$$

$$\text{Total Weight } (W_T) = \rho_w \times \text{Volume}_{\text{total}} = 35.47 \times 2.02 = 71.8 \text{ lbs}$$

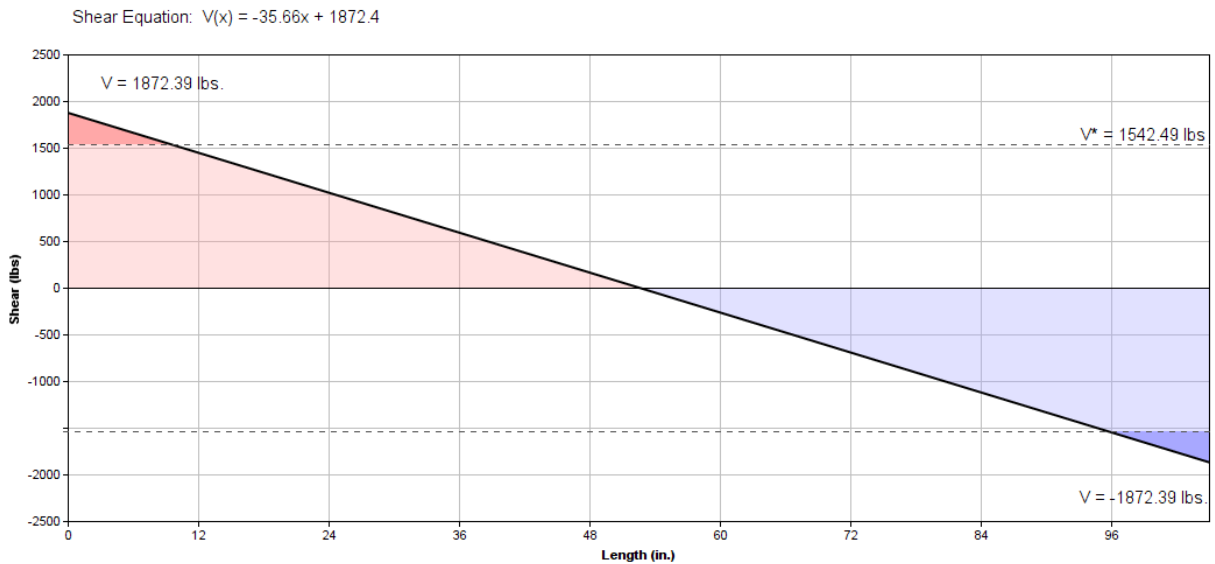
$$\text{Self Weight } (W_S) = \rho_w \times \text{Volume}_{\text{span}} = 35.47 \times 1.97 = 69.8 \text{ lbs}$$

$$\text{Distributed Self Weight } (w_s) = 7.97 \text{ plf}$$

Load, Shear and Moment Diagrams:



Beam - Shear Diagram

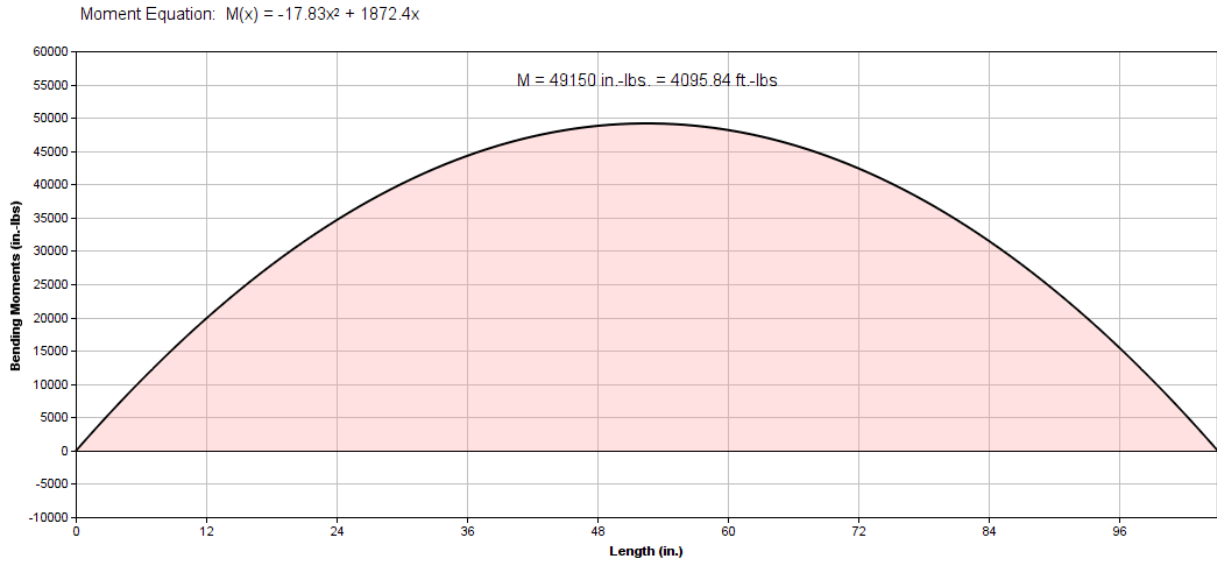


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**Beam - Moment Diagram**



1.) Bending:

Members subject to bending stresses shall be proportioned so that the actual bending stress or moment shall not exceed the adjusted bending design value:

$$f_b \leq F_b' \quad (NDS \text{ Sec. } 3.3.1)$$

where:

$$f_b = M / S$$

$$F_b' = F_b(C_D)(C_M)(C_t)(C_L)(C_F)(C_i)(C_r)$$

Beam is unbraced along its compression edge, lateral stability is considered below:

Slenderness Ratio for bending member RB:

$$l_u = \text{Unbraced Length} = 8.750 \text{ ft.}$$

$$l_u/d = 11.35$$

$$l_e = 1.63l_u + 3d = 1.63(105.0) + 3(9.25) = 198.90 \text{ in.} = 16.57 \text{ ft.} \quad (NDS \text{ Table } 3.3.3)$$

$$R_b = 12.26$$

$$R_b = 12.26 < 50 \quad ? \quad \mathbf{OK}$$

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Euler-based ASD critical buckling value for bending members:

$$E_{\min y'} = E_{\min y}(C_M)(C_t)(C_i) = 580000(0.9)(1)(0.95) = 495900 \text{ psi}$$

$$F_{bE} = = 3962.19 \text{ psi}$$

$$F_{bx}^* = F_{bx}(C_D)(C_M)(C_t)(C_F)(C_i)(C_r) = (900)(1.15)(1)(1)(1.2)(0.8)(1.15) = 1142.64 \text{ psi}$$

Beam stability factor:

$$C_L = = 0.981$$

$$F_{bx}' = (900)(1.15)(1)(1)(0.981)(1.2)(0.8)(1.15) = 1120.5 \text{ psi}$$

$$f_b = = 984.7 \text{ psi}$$

$$f_b = 984.7 \text{ psi} < F_{bx}' = 1120.5 \text{ psi} \quad (\text{CSI} = 0.88) \quad ? \quad \mathbf{OK}$$

## 2.) Shear:

Members subject to shear stresses shall be proportioned so that the actual shear stress parallel to grain or shear force at any cross section of the bending member shall not exceed the adjusted shear design value:

$$f_v \leq F_v' \quad (\text{NDS Sec. 3.4.1})$$

where:

$$f_v =$$

$$F_v' = F_v(C_D)(C_M)(C_t)(C_i)$$

$$F_{vx}' = (180)(1.15)(0.97)(1)(0.8) = 160.63 \text{ psi}$$

Shear Reduction: Uniformly distributed loads within a distance,  $d$ , from supports equal to the depth of the bending member shall be permitted to be ignored. Concentrated loads within a distance equal to the depth of the bending member from supports shall be permitted to be multiplied by  $x/d$  where  $x$  is the distance from the beam support face to the load. See NDS 2015, Figure 3C.

$$f_v^* = = 71.47 \text{ psi}$$

$$f_v^* = 71.47 \text{ psi} < F_{vx}' = 160.63 \text{ psi} \quad (\text{CSI} = 0.44) \quad ? \quad \mathbf{OK}$$

No Reduction in Shear (conservative):

$$f_v = = 86.75 \text{ psi}$$

$$f_v = 86.75 \text{ psi} < F_{vx}' = 160.63 \text{ psi} \quad (\text{CSI} = 0.54) \quad ? \quad \mathbf{OK}$$

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### 3.) Deflection:

Bending deflections calculated per standard method of engineering mechanics for live load and total load:

LL Allowable:  $L/360$

TL Allowable:  $L/240$

$$E_x' = E_x(C_M)(C_t)(C_i) = 1600000(0.9)(1)(0.95) = 1368000 \text{ psi}$$

$$\Delta_{LL} = 0.15 \text{ in.}$$

$$(L/d)_{LL} = 105.00 / 0.15 = 698$$

$$\Delta_{LL} = 0.15 \text{ in} = L/698 < L/360 \quad ? \text{ OK}$$

$$\Delta_{TL} = 0.18 \text{ in.}$$

$$(L/d)_{TL} = 105.00 / 0.18 = 587$$

$$\Delta_{TL} = 0.18 \text{ in} = L/587 < L/240 \quad ? \text{ OK}$$

### 4.) Bearing:

Members subject to bearing stresses perpendicular to the grain shall be proportioned so that the actual compressive stress perpendicular to grain shall be based on the net bearing area and shall not exceed the adjusted compression design value perpendicular to grain:

$$f_{c \perp} \leq F_{c \perp}' \quad (\text{NDS Sec. 3.10.2})$$

where:

$$f_{c \perp} =$$

$$F_{c \perp}' = F_{c \perp}(C_M)(C_t)(C_i)$$

$$F_{c \perp}' = (625)(0.67)(1)(1) = 418.75 \text{ psi}$$

$$A_b = b \times l_b = 3.5 \times 3 = 10.50 \text{ in}^2$$

$$f_{c \perp} = 183.4 \text{ psi}$$

$$f_{c \perp} = 183.4 \text{ psi} < F_{c \perp}' = 418.75 \text{ psi} \quad (\text{CSI} = 0.44) \quad ? \text{ OK}$$

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