

*Notes: 1.) Shear Distribution based on equivalent deflection of each shear panel.

2.) Holdown forces shown in grey indicate loads if holdowns assume 100% of shear panel overturning moments.

3.) Holdown forces conservative since counteracting dead loads (LC7: 0.6D + 0.6W) are not considered in analysis.

Design Criteria:	000 ll -					Job#:	2015-036
Max. Shear @ Panels =	900 lbs			.			
Max. Panel Width =	1.333 ft.				ng Panel Thickness =	7/16 in	
Max. Unit Shear @ Panels =	675.0 plf				ugh Thickness: F _v t _v =	165 lbs/in.	
				S	heathing both sides :	NO	
Moment Distribution:					Nail Spacing: S =	3 in.	
Max. Moments @ Panels =	75,600 in-lbs				Fastener Type :	8d	
Applied Moment @ Top of Shear Panel =	43,348 in-lbs	57%		Fastener Later	al Design Value: Z =	73 lbs (tab	LE 11Q, 2012 NDS)
Applied Moment @ Bottom of Shear Panel = 32,252 in-lbs		43%					
					Header Depth =	9.25 in.	
Shear Capacity of Sheathing (Shear-through-Thickne	ess):				Header Strap :	MSTC28	(Simpson)
Adjusted Panel Shear through Thickness: $F_v t_v' = F_v$	$\overline{t_v(C_D)(C_M)(C_t)(C_G)} =$		3,168 plf	Header Strap	Allowable Tension =	3,455 lbs -	—> ок
-	———————————————— ок				der Strap both sides :	NO	
Shear Capacity of Panel-to-Framing Nails:					Holdowns :	STHD14	(Simpson)
Number of Nails (based on two rows at 3" o/c) =			12.0 nails	Holdown	Allowable Tension =	3,200 lbs -	
Adjusted Lateral Capacity of Nails: $Z' = Z(C_D)(N) =$			1,402 lbs	Totoown	Shear Panel Posts :	(2) 2x6	
1,402 lbs > 900 lbs	> ок		1,102 100	Shoor Don	el Posts Thickness =	3.00 in.	
1,402 IDS > 900 IDS				Shear Fan		3.00	
Sheer Capacity of Apphar Dalta				Lood		1.6 (Seism	ic/Mind)
Shear Capacity of Anchor Bolts:			1.712 lbs	Luau I	Duration Factor: $C_D =$	1.6 (Seisin	iic/ williu)
Adjusted Lateral Capacity of Bolts: $Z_{ab}' = Z_{ab}(C_D)(N)$			1,712 105			(0) 0	
1,712 lbs > 900 lbs	──── ОК				Sill Plate:	(3)-2x	
				Number of And	chor Bolts per Panel =	1	
Moment Capacity of Sheathing (Edgewise Bending @ Header/Top of Panel):					Anchor Bolt DIA =		
Section Modulus of Sheathing Panel in Bending: $S = bh^2/6 =$			18.67 in. ³	AB Lateral Design Value: $Z_{ab} = 1,070$ lbs (TABLE 11E, 2012 N		LE 11E, 2012 NDS)	
Adjusted Moment Capacity of Sheathing: $M_{wsp}' = F_{t}$	$_{\rm pe}(C_{\rm D})(S) =$		17,920 in-lbs				
				Allowable Edgewise Bending Stress: F _{be} = 600 psi (TABLE 4, APA W345)			LE 4, APA W345)
Moment Capacity of Header Strap (Tension @ Header/Top of Panel):				Foundation Type = 6" Stemwall			
Adjusted Moment Capacity of Header Strap: $M_{strap}' = T_{strap}(W_p - 1.5) =$			50,098 in-Ibs	098 in-Ibs			
Moment Capacity of Nails into Header: (nail spacing @ 3 x 3 grid pattern)							
Distance from center of rotation to furthest fastener (longest moment arm): r _{max} =			7.57 in. (assume nail edge distance of 0.75")				
Polar Moment of Inertia of Nail Group: $J = I_x + I_y = bh^3/12 + hb^3/12 =$			5,326 in.4	-			
Adjusted Moment Capacity of Header Nail Group: M			9,133 in-lbs				
··			-,				
Combined Moment Capacity at Top of Portal Frame	Shear Panel =		59,231 in-lbs	>	43.348 in-lbs	→ ок	
			, -		-,		
Moment Capacity of Holdown:							
Distance from centerline of holdown to panel edge: 1	D		3 in.				
Adjusted Moment Capacity of Holdown: M _{holdown} ' = ⁻	Contor		41,600 in-lbs	>	30,445 in-lbs —	→ ок	
Adjusted Merrent Capacity of Holdown. Wholdown -	noldown(**p Center) -		41,000 11103		50,445 11 155		
Moment Capacity of Nails into Sill Plate: (only nails into bottom sill plate considered, conservative)							
Polar Moment of Inertia of Nail Group: $J = I_x + I_y = bh^3/12 + bb^3/12 =$			7.25 in. (assume nail edge distance of 0.75") 1.379 in. ⁴				
Polar Moment of Inertia of Nail Group: $J = I_x + I_y = bh^2/12 + hb^2/12 =$ Adjusted Moment Capacity of Sill Plate Nail Group: $M_{sill}' = ZC_D J/S^2 r_{max} =$,				
Adjusted Moment Capacity of SIII Plate Nail Group:	$IVI_{sill} = 2C_D J/S^{-} I_{max} =$		2,469 in-lbs				
Combined Moment Capacity at Bottom of Portal Fran	ne Shear Panel =		44,069 in-lbs	>	32,252 in-lbs	→ ок	