2010 Edition of ASCE 7
Minimum Design Loads for Buildings and Other Structures
Errata No.2

Effective: March 31, 2013

This document contains errata to ASCE 7-10 and is periodically updated and posted on the SEI website at www.asce.org/sei/errata.

THIS TYPE AND SIZE FONT INDICATES DIRECTIVE TEXT THAT IS NOT PART OF THE STANDARD. CHANGES TO THE STANDARD ARE INDICATED USING STRIKE-OUT AND UNDERLINE TEXT.

Chapter 4

REVISE TABLE 4-1 AS FOLLOWS:

Occupancy or Use	Uniform psf (kN/m^2)	Conc. lb (kN)
Screen enclosure support frame	5 (0.24) nonreducible and based on the tributary area of the roof supported by the frame members	200 (0.89)

4.7.2 Reduction in Uniform Live Loads.

…

~~**EXCEPTION:** For structural members in one- and two-family dwellings supporting more than one floor load, the following floor live load reduction shall be permitted as an alternative to Eq. 4.7-1:~~

$$~~L = 0.7 \times (L_{o1} + L_{o2} + \ldots)~~$$

~~L_{o1}, L_{o2}, … are the unreduced floor live loads applicable to each of multiple supported story levels regardless of tributary area. The reduced floor live load effect, L, shall not be less than that produced by the effect of the largest unreduced floor live load on a given story level acting alone.~~

Chapter 7

7.4.2 Cold Roof Slope Factor, Cs.

Cold roofs are those with a $Ct > 1.0$ as determined from Table 7-3. For cold roofs with $Ct = 1.1$ and an unobstructed slippery surface that will allow snow to slide off the eaves, the roof slope factor Cs shall be determined using the dashed line in Fig. 7-2b. For all other cold roofs with$Ct = 1.1$, the solid line in Fig. 7-2b shall be used to determine the roof slope factor Cs. For cold roofs with $Ct = 1.2$ or larger and an unobstructed slippery surface that will allow snow to slide off the eaves, the roof slope factor Cs shall be determined using the dashed line on Fig. 7-2c. For all other cold roofs with $Ct = 1.2$ or larger, the solid line in Fig. 7-2c shall be used to determine the roof slope factor Cs.

REVISE FIGURE 7-5 TO CHANGE “W < 20 FT” TO “W ≤ 20 FT” AND “Θ ≤ 2.38°” TO “Θ < 2.38°”

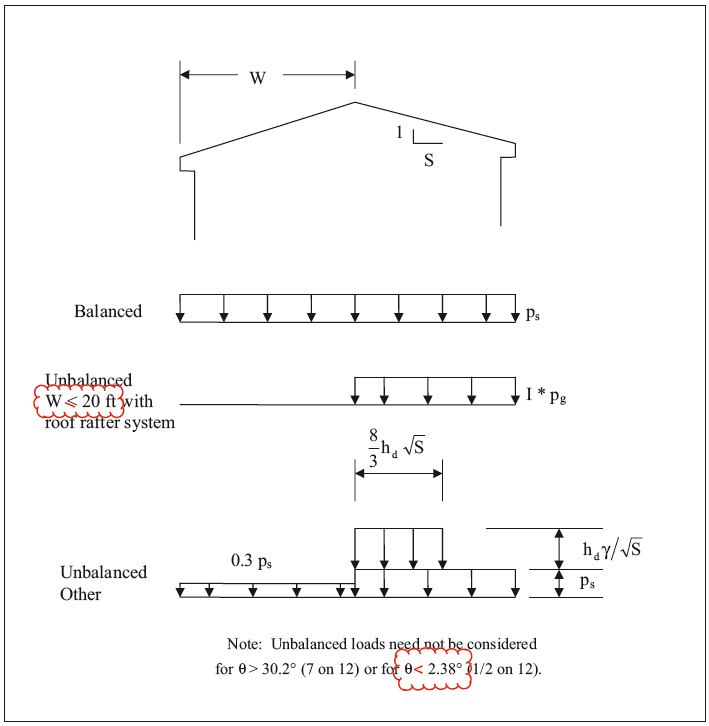
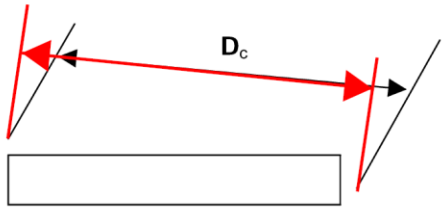


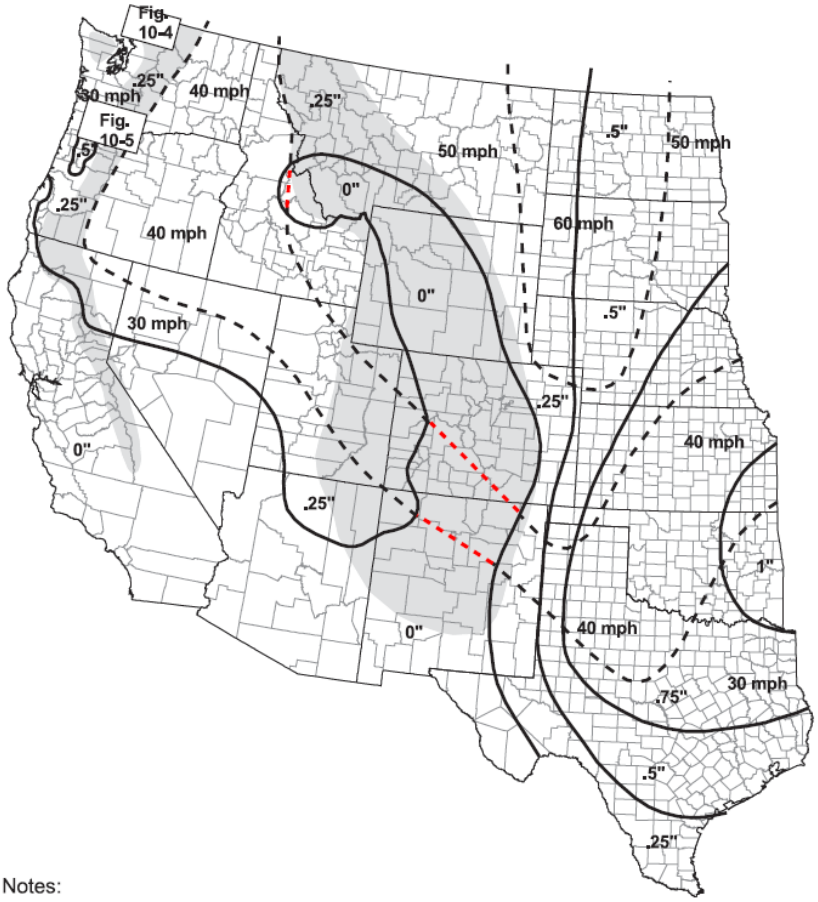
FIGURE 7-5 Balanced and Unbalanced Snow Loads for Hip and Gable Roofs.

Chapter 10

REVISE FIGURE 10-1 RECTANGULAR SHAPE TO SHOW DIMENSION LINE PERPENDICULAR TO THE EXTENSION LINES.



REVISE FIGURE 10-2 TO CONNECT GUST SPEED CONTOURS IDAHO, COLORADO AND NEW MEXICO AS SHOWN IN RED BELOW.



Notes:

Chapter 12

REVISE THE REFERENCE TO ACI 318 UNDER THE EXCEPTION IN SECTION 12.12.5 TO READ:

EXCEPTION: Reinforced concrete frame members not designed as part of the seismic force–resisting system shall comply with Section ~~21.11~~ 21.13 of ACI 318.

REVISE TABLE 12.6-1 TO DELETE THE "TYPE 5B" ENTRY UNDER THE STRUCTURAL CHARACTERISTICS COLUMN. SECTION 12.3.3.1 PROHIBITS VERTICAL IRREGULARITY TYPE 5B IN STRUCTURES ASSIGNED TO SDC D OR HIGHER.

REVISE SECTION 12.14.3.1.2 EXCEPTION CONDITION 1 AS FOLLOWS:

1. In Eqs. 12.14-3, 12.14-4, 12.14-7, and 12.14-8 where SDS is equal to or less than 0.125.

Chapter 15

15.4.4 Fundamental Period.

…

~~$T = 2\pi \sqrt{\frac{\sum_{i=1}^{n} f_i \delta_i^2}{g \sum_{i=1}^{n} f_i \delta_i}}$~~

$$T = 2\pi \sqrt{\frac{\sum_{i=1}^{n} w_i \delta_i^2}{g \sum_{i=1}^{n} f_i \delta_i}} \qquad (15.4\text{-}6)$$

Chapter 16

16.1.4 Response Parameters.

REVISE PARAGRAPH 2 AS FOLLOWS:

For each ground motion *i*, where *i* is the designation assigned to each ground motion, the maximum value of the base shear, V_i, member forces, Q_{Ei}, and story drifts, Δ_i at each story, scaled as indicated in the preceding text ~~and story drifts, Δ_i, at each story as defined in Section 12.8.6~~ shall be determined. Where the maximum scaled base shear predicted by the analysis, V_i, is less than 85 percent of the value of V determined using the minimum value of C_s set forth in Eq. 12.8-5 or when located where S_1 is equal to or greater than 0.6*g*, the minimum value of C_s set forth in Eq. 12.8-6, the scaled member forces,

Q_{Ei}, shall be additionally multiplied by $0.85\frac{V}{V_i}$ where V is

the minimum base shear that has been determined using the minimum value of C_s set forth in Eq. 12.8-5, or when located where S_1 is equal to or greater than 0.6*g*, the minimum value of C_s set forth in Eq. 12.8-6.

REMAINDER OF THE SECTION IS UNCHANGED.

Chapter 22

REPLACE FIGURES 22-7 TO 22-9 WITH NEW MCE_G PGA MAPS THAT REVISE, FROM 60% g TO 50% g, SHADED AREAS OF DETERMINISTIC LOWER LIMIT PEAK GROUND ACCELERATIONS FOR THE CONTERMINOUS UNITED STATES, ALASKA, AND HAWAII. MAPS ARE APPENDED TO THE END OF THIS ERRATUM.

Chapter 23

ADD EDITION DATETO AWWA D100 TO AVOID CONFUSION. COPYRIGHT IS 2006, EDITION IS 2005.

AWWA D100-05
Sections 15.4.1, 15.7.7.1, 15.7.9.4, 15.7.10.6
Welded Steel Tanks for Water Storage, 2006

Chapter 26

FIGURES 26.5-1A, FIGURE 26.5B, FIGURE 26.5-1C

Notes:
1. Values are ~~nominal~~ design 3-second gust wind speeds in miles per hour (m/s) at 33 ft (10m) above ground for Exposure C category.

EQUATION 26.11-1 IN THE DENOMINATOR CHANGE “22.800” TO “22,800”.

Chapter 27

Table 27.2-1 Steps to Determine MWFRS Wind Loads for Enclosed, Partially Enclosed, and Open Buildings of All Heights
Step 1: Determine risk category of building or other structure, see Table ~~1.4-1~~ 1.5-1.

Table 27.5-1 Steps to Determine MWFRS Wind Loads Enclosed Simple Diaphragm Buildings ($h \leq 160$ ft. (48.8 m))

Step 1: Determine risk category of building or other structure, see Table 1.5-1
Step 2: Determine the basic wind speed, *V*, for applicable risk category, see Figure 26.5-1A, B or C
Step 3: Determine wind load parameters:

- ~~Wind directionality factor, Kd, see Section 26.6 and Table 26.6-1~~
- Exposure category B, C or D, see Section 26.7
- Topographic factor, Kzt, see Section 26.8 and Figure 26.8-1
- Enclosure classification, see Section 26.10

Table 27.6-2 MWFRS- Part 2: Wind Loads – Roof Exposure C

FOR V = 160–200 MPH, ALL HEIGHTS, REPLACE MULIPLE VALUES FOR 160 MPH, ZONE 2, LOAD CASE 1.

Table 27.6-2
MWFRS- Part 2: Wind Loads - Roof Exposure C

MWFRS – Roof
V = 160–200 mph
h = 50–80 ft.

V (MPH)			160					180					200				
		Load			Zone					Zone					Zone		
h (ft)	Roof Slope	Case	1	2	3	4	5	1	2	3	4	5	1	2	3	4	5
80	Flat < 2:12 (9.46 deg)	1	NA	NA	-71.3	-63.6	-52.1	NA	NA	-90.2	-80.5	-66.0	NA	NA	-111.4	-99.3	-81.5
		2	NA	NA	0.0	0.0	0.0	NA	NA	0.0	0.0	0.0	NA	NA	0.0	0.0	0.0
	3:12 (14.0 deg)	1	-70.0	-47.6	-71.3	-63.6	-52.1	-88.5	-60.2	-90.2	-80.5	-66.0	-109.3	-74.3	-111.4	-99.3	-81.5
		2	10.1	-14.2	0.0	0.0	0.0	12.8	-18.0	0.0	0.0	0.0	15.8	-22.2	0.0	0.0	0.0
	4:12 (18.4 deg)	1	-57.5	-46.4	-71.3	-63.6	-52.1	-72.8	-58.7	-90.2	-80.5	-66.0	-89.9	-72.5	-111.4	-99.3	-81.5
		2	19.9	-20.4	0.0	0.0	0.0	25.2	-25.8	0.0	0.0	0.0	31.1	-31.8	0.0	0.0	0.0
	5:12 (22.6 deg)	1	-46.1	-46.4	-71.3	-63.6	-52.1	-58.4	-58.7	-90.2	-80.5	-66.0	-72.1	-72.5	-111.4	-99.3	-81.5
		2	26.5	-22.2	0.0	0.0	0.0	33.5	-28.1	0.0	0.0	0.0	41.4	-34.7	0.0	0.0	0.0
	6:12 (26.6 deg)	1	-37.1	-46.4	-71.3	-63.6	-52.1	-46.9	-58.7	-90.2	-80.5	-66.0	-57.9	-72.5	-111.4	-99.3	-81.5
		2	29.3	-22.2	0.0	0.0	0.0	37.0	-28.1	0.0	0.0	0.0	45.7	-34.7	0.0	0.0	0.0
	9:12 (36.9 deg)	1	-21.5	-46.4	-71.3	-63.6	-52.1	-27.2	-58.7	-90.2	-80.5	-66.0	-33.5	-72.5	-111.4	-99.3	-81.5
		2	35.0	-22.2	0.0	0.0	0.0	44.3	-28.1	0.0	0.0	0.0	54.7	-34.7	0.0	0.0	0.0
	12:12 (45.0 deg)	1	-12.1	-46.4	-71.3	-63.6	-52.1	-15.3	-58.7	-90.2	-80.5	-66.0	-18.9	-72.5	-111.4	-99.3	-81.5
		2	35.0	-22.2	0.0	0.0	0.0	44.3	-28.1	0.0	0.0	0.0	54.7	-34.7	0.0	0.0	0.0
70	Flat < 2:12 (9.46 deg)	1	NA	NA	-69.3	-61.8	-50.7	NA	NA	-87.7	-78.2	-64.2	NA	NA	-108.3	-96.6	-79.2
		2	NA	NA	0.0	0.0	0.0	NA	NA	0.0	0.0	0.0	NA	NA	0.0	0.0	0.0
	3:12 (14.0 deg)	1	-68.0	-46.2	-69.3	-61.8	-50.7	-86.1	-58.5	-87.7	-78.2	-64.2	-106.3	-72.2	-108.3	-96.6	-79.2
		2	9.8	-13.8	0.0	0.0	0.0	12.4	-17.5	0.0	0.0	0.0	15.3	-21.6	0.0	0.0	0.0
	4:12 (18.4 deg)	1	-55.9	-45.1	-69.3	-61.8	-50.7	-70.8	-57.1	-87.7	-78.2	-64.2	-87.4	-70.5	-108.3	-96.6	-79.2
		2	19.4	-19.8	0.0	0.0	0.0	24.5	-25.1	0.0	0.0	0.0	30.2	-31.0	0.0	0.0	0.0
	5:12 (22.6 deg)	1	-44.9	-45.1	-69.3	-61.8	-50.7	-56.8	-57.1	-87.7	-78.2	-64.2	-70.1	-70.5	-108.3	-96.6	-79.2
		2	25.8	-21.6	0.0	0.0	0.0	32.6	-27.3	0.0	0.0	0.0	40.3	-33.7	0.0	0.0	0.0
	6:12 (26.6 deg)	1	-36.0	-45.1	-69.3	-61.8	-50.7	-45.6	-57.1	-87.7	-78.2	-64.2	-56.3	-70.5	-108.3	-96.6	-79.2
		2	28.4	-21.6	0.0	0.0	0.0	36.0	-27.3	0.0	0.0	0.0	44.5	-33.7	0.0	0.0	0.0
	9:12 (36.9 deg)	1	-20.9	-45.1	-69.3	-61.8	-50.7	-26.4	-57.1	-87.7	-78.2	-64.2	-32.6	-70.5	-108.3	-96.6	-79.2
		2	34.0	-21.6	0.0	0.0	0.0	43.0	-27.3	0.0	0.0	0.0	53.1	-33.7	0.0	0.0	0.0
	12:12 (45.0 deg)	1	-11.8	-45.1	-69.3	-61.8	-50.7	-14.9	-57.1	-87.7	-78.2	-64.2	-18.4	-70.5	-108.3	-96.6	-79.2
		2	34.0	-21.6	0.0	0.0	0.0	43.0	-27.3	0.0	0.0	0.0	53.1	-33.7	0.0	0.0	0.0
60	Flat < 2:12 (9.46 deg)	1	NA	NA	-67.1	-59.8	-49.1	NA	NA	-84.9	-75.7	-62.1	NA	NA	-104.9	-93.5	-76.7
		2	NA	NA	0.0	0.0	0.0	NA	NA	0.0	0.0	0.0	NA	NA	0.0	0.0	0.0
	3:12 (14.0 deg)	1	-65.8	-44.8	-67.1	-59.8	-49.1	-83.3	-56.7	-84.9	-75.7	-62.1	-102.9	-69.9	-104.9	-93.5	-76.7
		2	9.5	-13.4	0.0	0.0	0.0	12.0	-16.9	0.0	0.0	0.0	14.8	-20.9	0.0	0.0	0.0
	4:12 (18.4 deg)	1	-54.1	-43.7	-67.1	-59.8	-49.1	-68.5	-55.3	-84.9	-75.7	-62.1	-84.6	-68.3	-104.9	-93.5	-76.7
		2	18.7	-19.2	0.0	0.0	0.0	23.7	-24.3	0.0	0.0	0.0	29.3	-30.0	0.0	0.0	0.0
	5:12 (22.6 deg)	1	-43.4	-43.7	-67.1	-59.8	-49.1	-55.0	-55.3	-84.9	-75.7	-62.1	-67.9	-68.3	-104.9	-93.5	-76.7
		2	24.9	-20.9	0.0	0.0	0.0	31.6	-26.4	0.0	0.0	0.0	39.0	-32.6	0.0	0.0	0.0
	6:12 (26.6 deg)	1	-34.9	-43.7	-67.1	-59.8	-49.1	-44.2	-55.3	-84.9	-75.7	-62.1	-54.5	-68.3	-104.9	-93.5	-76.7
		2	27.5	-20.9	0.0	0.0	0.0	34.9	-26.4	0.0	0.0	0.0	43.0	-32.6	0.0	0.0	0.0
	9:12 (36.9 deg)	1	-20.2	-43.7	-67.1	-59.8	-49.1	-25.6	-55.3	-84.9	-75.7	-62.1	-31.6	-68.3	-104.9	-93.5	-76.7
		2	32.9	-20.9	0.0	0.0	0.0	41.7	-26.4	0.0	0.0	0.0	51.4	-32.6	0.0	0.0	0.0
	12:12 (45.0 deg)	1	-11.4	-43.7	-67.1	-59.8	-49.1	-14.4	-55.3	-84.9	-75.7	-62.1	-17.8	-68.3	-104.9	-93.5	-76.7
		2	32.9	-20.9	0.0	0.0	0.0	41.7	-26.4	0.0	0.0	0.0	51.4	-32.6	0.0	0.0	0.0
50	Flat < 2:12 (9.46 deg)	1	NA	NA	-64.6	-57.6	-47.2	NA	NA	-81.7	-72.9	-59.8	NA	NA	-100.9	-90.0	-73.8
		2	NA	NA	0.0	0.0	0.0	NA	NA	0.0	0.0	0.0	NA	NA	0.0	0.0	0.0
	3:12 (14.0 deg)	1	-63.4	-43.1	-64.6	-57.6	-47.2	-80.2	-54.5	-81.7	-72.9	-59.8	-99.0	-67.3	-100.9	-90.0	-73.8
		2	9.1	-12.9	0.0	0.0	0.0	11.6	-16.3	0.0	0.0	0.0	14.3	-20.1	0.0	0.0	0.0
	4:12 (18.4 deg)	1	-52.1	-42.0	-64.6	-57.6	-47.2	-65.9	-53.2	-81.7	-72.9	-59.8	-81.4	-65.7	-100.9	-90.0	-73.8
		2	18.0	-18.5	0.0	0.0	0.0	22.8	-23.4	0.0	0.0	0.0	28.2	-28.8	0.0	0.0	0.0
	5:12 (22.6 deg)	1	-41.8	-42.0	-64.6	-57.6	-47.2	-52.9	-53.2	-81.7	-72.9	-59.8	-65.3	-65.7	-100.9	-90.0	-73.8
		2	24.0	-20.1	0.0	0.0	0.0	30.4	-25.4	0.0	0.0	0.0	37.5	-31.4	0.0	0.0	0.0
	6:12 (26.6 deg)	1	-33.6	-42.0	-64.6	-57.6	-47.2	-42.5	-53.2	-81.7	-72.9	-59.8	-52.5	-65.7	-100.9	-90.0	-73.8
		2	26.5	-20.1	0.0	0.0	0.0	33.5	-25.4	0.0	0.0	0.0	41.4	-31.4	0.0	0.0	0.0
	9:12 (36.9 deg)	1	-19.4	-42.0	-64.6	-57.6	-47.2	-24.6	-53.2	-81.7	-72.9	-59.8	-30.4	-65.7	-100.9	-90.0	-73.8
		2	31.7	-20.1	0.0	0.0	0.0	40.1	-25.4	0.0	0.0	0.0	49.5	-31.4	0.0	0.0	0.0
	12:12 (45.0 deg)	1	-11.0	-42.0	-64.6	-57.6	-47.2	-13.9	-53.2	-81.7	-72.9	-59.8	-17.1	-65.7	-100.9	-90.0	-73.8
		2	31.7	-20.1	0.0	0.0	0.0	40.1	-25.4	0.0	0.0	0.0	49.5	-31.4	0.0	0.0	0.0

Table 27.6-2
MWFRS- Part 2: Wind Loads - Roof
Exposure C

MWFRS – Roof
V = 160–200 mph
h = 90–120 ft.

V (MPH)			160					180					200				
		Load			Zone					Zone					Zone		
h (ft)	Roof Slope	Case	1	2	3	4	5	1	2	3	4	5	1	2	3	4	5
120	Flat < 2:12 (9.46 deg)	1	NA	NA	-77.7	-69.2	-56.8	NA	NA	-98.3	-87.6	-71.9	NA	NA	-121.3	-108.2	-88.7
		2	NA	NA	0.0	0.0	0.0	NA	NA	0.0	0.0	0.0	NA	NA	0.0	0.0	0.0
	3:12 (14.0 deg)	1	-76.2	-51.8	-77.7	-69.2	-56.8	-96.4	-65.6	-98.3	-87.6	-71.9	-119.0	-80.9	-121.3	-108.2	-88.7
		2	11.0	-15.5	0.0	0.0	0.0	13.9	-19.6	0.0	0.0	0.0	17.2	-24.2	0.0	0.0	0.0
	4:12 (18.4 deg)	1	-62.6	-50.5	-77.7	-69.2	-56.8	-79.3	-64.0	-98.3	-87.6	-71.9	-97.9	-79.0	-121.3	-108.2	-88.7
		2	21.7	-22.2	0.0	0.0	0.0	27.4	-28.1	0.0	0.0	0.0	33.9	-34.7	0.0	0.0	0.0
	5:12 (22.6 deg)	1	-50.3	-50.5	-77.7	-69.2	-56.8	-63.6	-64.0	-98.3	-87.6	-71.9	-78.5	-79.0	-121.3	-108.2	-88.7
		2	28.9	-24.2	0.0	0.0	0.0	36.5	-30.6	0.0	0.0	0.0	45.1	-37.8	0.0	0.0	0.0
	6:12 (26.6 deg)	1	-40.4	-50.5	-77.7	-69.2	-56.8	-51.1	-64.0	-98.3	-87.6	-71.9	-63.1	-79.0	-121.3	-108.2	-88.7
		2	31.9	-24.2	0.0	0.0	0.0	40.3	-30.6	0.0	0.0	0.0	49.8	-37.8	0.0	0.0	0.0
	9:12 (36.9 deg)	1	-23.4	-50.5	-77.7	-69.2	-56.8	-29.6	-64.0	-98.3	-87.6	-71.9	-36.5	-79.0	-121.3	-108.2	-88.7
		2	38.1	-24.2	0.0	0.0	0.0	48.2	-30.6	0.0	0.0	0.0	59.5	-37.8	0.0	0.0	0.0
	12:12 (45.0 deg)	1	-13.2	-50.5	-77.7	-69.2	-56.8	-16.7	-64.0	-98.3	-87.6	-71.9	-20.6	-79.0	-121.3	-108.2	-88.7
		2	38.1	-24.2	0.0	0.0	0.0	48.2	-30.6	0.0	0.0	0.0	59.5	-37.8	0.0	0.0	0.0
110	Flat < 2:12 (9.46 deg)	1	NA	NA	-76.2	-68.0	-55.7	NA	NA	-96.5	-86.0	-70.6	NA	NA	-119.1	-106.2	-87.1
		2	NA	NA	0.0	0.0	0.0	NA	NA	0.0	0.0	0.0	NA	NA	0.0	0.0	0.0
	3:12 (14.0 deg)	1	-74.8	-50.9	-76.2	-68.0	-55.7	-94.7	-64.4	-96.5	-86.0	-70.6	-116.9	-79.5	-119.1	-106.2	-87.1
		2	10.8	-15.2	0.0	0.0	0.0	13.7	-19.2	0.0	0.0	0.0	16.9	-23.7	0.0	0.0	0.0
	4:12 (18.4 deg)	1	-61.5	-49.6	-76.2	-68.0	-55.7	-77.8	-62.8	-96.5	-86.0	-70.6	-96.1	-77.6	-119.1	-106.2	-87.1
		2	21.3	-21.8	0.0	0.0	0.0	26.9	-27.6	0.0	0.0	0.0	33.3	-34.1	0.0	0.0	0.0
	5:12 (22.6 deg)	1	-49.3	-49.6	-76.2	-68.0	-55.7	-62.5	-62.8	-96.5	-86.0	-70.6	-77.1	-77.6	-119.1	-106.2	-87.1
		2	28.3	-23.7	0.0	0.0	0.0	35.9	-30.0	0.0	0.0	0.0	44.3	-37.1	0.0	0.0	0.0
	6:12 (26.6 deg)	1	-39.6	-49.6	-76.2	-68.0	-55.7	-50.2	-62.8	-96.5	-86.0	-70.6	-61.9	-77.6	-119.1	-106.2	-87.1
		2	31.3	-23.7	0.0	0.0	0.0	39.6	-30.0	0.0	0.0	0.0	48.9	-37.1	0.0	0.0	0.0
	9:12 (36.9 deg)	1	-22.9	-49.6	-76.2	-68.0	-55.7	-29.0	-62.8	-96.5	-86.0	-70.6	-35.9	-77.6	-119.1	-106.2	-87.1
		2	37.4	-23.7	0.0	0.0	0.0	47.3	-30.0	0.0	0.0	0.0	58.4	-37.1	0.0	0.0	0.0
	12:12 (45.0 deg)	1	-12.9	-49.6	-76.2	-68.0	-55.7	-16.4	-62.8	-96.5	-86.0	-70.6	-20.2	-77.6	-119.1	-106.2	-87.1
		2	37.4	-23.7	0.0	0.0	0.0	47.3	-30.0	0.0	0.0	0.0	58.4	-37.1	0.0	0.0	0.0
100	Flat < 2:12 (9.46 deg)	1	NA	NA	-74.7	-66.6	-54.6	NA	NA	-94.6	-84.3	-69.2	NA	NA	-116.8	-104.1	-85.4
		2	NA	NA	0.0	0.0	0.0	NA	NA	0.0	0.0	0.0	NA	NA	0.0	0.0	0.0
	3:12 (14.0 deg)	1	-73.3	-49.9	-74.7	-66.6	-54.6	-92.8	-63.1	-94.6	-84.3	-69.2	-114.6	-77.9	-116.8	-104.1	-85.4
		2	10.6	-14.9	0.0	0.0	0.0	13.4	-18.8	0.0	0.0	0.0	16.5	-23.2	0.0	0.0	0.0
	4:12 (18.4 deg)	1	-60.3	-48.6	-74.7	-66.6	-54.6	-76.3	-61.6	-94.6	-84.3	-69.2	-94.2	-76.0	-116.8	-104.1	-85.4
		2	20.9	-21.4	0.0	0.0	0.0	26.4	-27.0	0.0	0.0	0.0	32.6	-33.4	0.0	0.0	0.0
	5:12 (22.6 deg)	1	-48.4	-48.6	-74.7	-66.6	-54.6	-61.2	-61.6	-94.6	-84.3	-69.2	-75.6	-76.0	-116.8	-104.1	-85.4
		2	27.8	-23.3	0.0	0.0	0.0	35.2	-29.4	0.0	0.0	0.0	43.4	-36.4	0.0	0.0	0.0
	6:12 (26.6 deg)	1	-38.8	-48.6	-74.7	-66.6	-54.6	-49.2	-61.6	-94.6	-84.3	-69.2	-60.7	-76.0	-116.8	-104.1	-85.4
		2	30.7	-23.3	0.0	0.0	0.0	38.8	-29.4	0.0	0.0	0.0	47.9	-36.4	0.0	0.0	0.0
	9:12 (36.9 deg)	1	-22.5	-48.6	-74.7	-66.6	-54.6	-28.5	-61.6	-94.6	-84.3	-69.2	-35.1	-76.0	-116.8	-104.1	-85.4
		2	36.7	-23.3	0.0	0.0	0.0	46.4	-29.4	0.0	0.0	0.0	57.3	-36.4	0.0	0.0	0.0
	12:12 (45.0 deg)	1	-12.7	-48.6	-74.7	-66.6	-54.6	-16.1	-61.6	-94.6	-84.3	-69.2	-19.8	-76.0	-116.8	-104.1	-85.4
		2	36.7	-23.3	0.0	0.0	0.0	46.4	-29.4	0.0	0.0	0.0	57.3	-36.4	0.0	0.0	0.0
90	Flat < 2:12 (9.46 deg)	1	NA	NA	-73.1	-65.2	-53.4	NA	NA	-92.5	-82.5	-67.6	NA	NA	-114.2	-101.8	-83.5
		2	NA	NA	0.0	0.0	0.0	NA	NA	0.0	0.0	0.0	NA	NA	0.0	0.0	0.0
	3:12 (14.0 deg)	1	-71.7	-48.8	-73.1	-65.2	-53.4	-90.8	-61.7	-92.5	-82.5	-67.6	-112.1	-76.2	-114.2	-101.8	-83.5
		2	10.3	-14.5	0.0	0.0	0.0	13.1	-18.4	0.0	0.0	0.0	16.2	-22.7	0.0	0.0	0.0
	4:12 (18.4 deg)	1	-59.0	-47.6	-73.1	-65.2	-53.4	-74.6	-60.2	-92.5	-82.5	-67.6	-92.1	-74.3	-114.2	-101.8	-83.5
		2	20.4	-20.9	0.0	0.0	0.0	25.8	-26.4	0.0	0.0	0.0	31.9	-32.6	0.0	0.0	0.0
	5:12 (22.6 deg)	1	-47.3	-47.6	-73.1	-65.2	-53.4	-59.9	-60.2	-92.5	-82.5	-67.6	-73.9	-74.3	-114.2	-101.8	-83.5
		2	27.2	-22.8	0.0	0.0	0.0	34.4	-28.8	0.0	0.0	0.0	42.5	-35.6	0.0	0.0	0.0
	6:12 (26.6 deg)	1	-38.0	-47.6	-73.1	-65.2	-53.4	-48.1	-60.2	-92.5	-82.5	-67.6	-59.4	-74.3	-114.2	-101.8	-83.5
		2	30.0	-22.8	0.0	0.0	0.0	38.0	-28.8	0.0	0.0	0.0	46.9	-35.6	0.0	0.0	0.0
	9:12 (36.9 deg)	1	-22.0	-47.6	-73.1	-65.2	-53.4	-27.8	-60.2	-92.5	-82.5	-67.6	-34.4	-74.3	-114.2	-101.8	-83.5
		2	35.9	-22.8	0.0	0.0	0.0	45.4	-28.8	0.0	0.0	0.0	56.0	-35.6	0.0	0.0	0.0
	12:12 (45.0 deg)	1	-12.4	-47.6	-73.1	-65.2	-53.4	-15.7	-60.2	-92.5	-82.5	-67.6	-19.4	-74.3	-114.2	-101.8	-83.5
		2	35.9	-22.8	0.0	0.0	0.0	45.4	-28.8	0.0	0.0	0.0	56.0	-35.6	0.0	0.0	0.0

Table 27.6-2
MWFRS – Part 2: Wind Loads – Roof
Exposure C

MWFRS – Roof
V = 160–200 mph
h = 130–160 ft.

V (MPH)			160					180					200				
		Load			Zone					Zone					Zone		
h (ft)	Roof Slope	Case	1	2	3	4	5	1	2	3	4	5	1	2	3	4	5
160	Flat < 2:12 (9.46 deg)	1	NA	NA	-82.5	-73.6	-60.3	NA	NA	-104.4	-93.1	-76.3	NA	NA	-128.9	-114.9	-94.3
		2	NA	NA	0.0	0.0	0.0	NA	NA	0.0	0.0	0.0	NA	NA	0.0	0.0	0.0
	3:12 (14.0 deg)	1	-80.9	-55.0	-82.5	-73.6	-60.3	-102.5	-69.6	-104.4	-93.1	-76.3	-126.5	-86.0	-128.9	-114.9	-94.3
		2	11.7	-16.4	0.0	0.0	0.0	14.8	-20.8	0.0	0.0	0.0	18.2	-25.7	0.0	0.0	0.0
	4:12 (18.4 deg)	1	-66.5	-53.7	-82.5	-73.6	-60.3	-84.2	-68.0	-104.4	-93.1	-76.3	-104.0	-83.9	-128.9	-114.9	-94.3
		2	23.0	-23.6	0.0	0.0	0.0	29.2	-29.8	0.0	0.0	0.0	36.0	-36.8	0.0	0.0	0.0
	5:12 (22.6 deg)	1	-53.4	-53.7	-82.5	-73.6	-60.3	-67.6	-68.0	-104.4	-93.1	-76.3	-83.4	-83.9	-128.9	-114.9	-94.3
		2	30.7	-25.7	0.0	0.0	0.0	38.8	-32.5	0.0	0.0	0.0	47.9	-40.1	0.0	0.0	0.0
	6:12 (26.6 deg)	1	-42.9	-53.7	-82.5	-73.6	-60.3	-54.3	-68.0	-104.4	-93.1	-76.3	-67.0	-83.9	-128.9	-114.9	-94.3
		2	33.9	-25.7	0.0	0.0	0.0	42.9	-32.5	0.0	0.0	0.0	52.9	-40.1	0.0	0.0	0.0
	9:12 (36.9 deg)	1	-24.8	-53.7	-82.5	-73.6	-60.3	-31.4	-68.0	-104.4	-93.1	-76.3	-38.8	-83.9	-128.9	-114.9	-94.3
		2	40.5	-25.7	0.0	0.0	0.0	51.2	-32.5	0.0	0.0	0.0	63.2	-40.1	0.0	0.0	0.0
	12:12 (45.0 deg)	1	-14.0	-53.7	-82.5	-73.6	-60.3	-17.7	-68.0	-104.4	-93.1	-76.3	-21.9	-83.9	-128.9	-114.9	-94.3
		2	40.5	-25.7	0.0	0.0	0.0	51.2	-32.5	0.0	0.0	0.0	63.2	-40.1	0.0	0.0	0.0
150	Flat < 2:12 (9.46 deg)	1	NA	NA	-81.4	-72.6	-59.5	NA	NA	-103.0	-91.8	-75.3	NA	NA	-127.2	-113.4	-93.0
		2	NA	NA	0.0	0.0	0.0	NA	NA	0.0	0.0	0.0	NA	NA	0.0	0.0	0.0
	3:12 (14.0 deg)	1	-79.9	-54.3	-81.4	-72.6	-59.5	-101.1	-68.7	-103.0	-91.8	-75.3	-124.8	-84.8	-127.2	-113.4	-93.0
		2	11.5	-16.2	0.0	0.0	0.0	14.6	-20.5	0.0	0.0	0.0	18.0	-25.3	0.0	0.0	0.0
	4:12 (18.4 deg)	1	-65.7	-53.0	-81.4	-72.6	-59.5	-83.1	-67.1	-103.0	-91.8	-75.3	-102.6	-82.8	-127.2	-113.4	-93.0
		2	22.7	-23.3	0.0	0.0	0.0	28.8	-29.4	0.0	0.0	0.0	35.5	-36.4	0.0	0.0	0.0
	5:12 (22.6 deg)	1	-52.7	-53.0	-81.4	-72.6	-59.5	-66.7	-67.1	-103.0	-91.8	-75.3	-82.3	-82.8	-127.2	-113.4	-93.0
		2	30.3	-25.3	0.0	0.0	0.0	38.3	-32.1	0.0	0.0	0.0	47.3	-39.6	0.0	0.0	0.0
	6:12 (26.6 deg)	1	-42.3	-53.0	-81.4	-72.6	-59.5	-53.5	-67.1	-103.0	-91.8	-75.3	-66.1	-82.8	-127.2	-113.4	-93.0
		2	33.4	-25.3	0.0	0.0	0.0	42.3	-32.1	0.0	0.0	0.0	52.2	-39.6	0.0	0.0	0.0
	9:12 (36.9 deg)	1	-24.5	-53.0	-81.4	-72.6	-59.5	-31.0	-67.1	-103.0	-91.8	-75.3	-38.3	-82.8	-127.2	-113.4	-93.0
		2	39.9	-25.3	0.0	0.0	0.0	50.5	-32.1	0.0	0.0	0.0	62.4	-39.6	0.0	0.0	0.0
	12:12 (45.0 deg)	1	-13.8	-53.0	-81.4	-72.6	-59.5	-17.5	-67.1	-103.0	-91.8	-75.3	-21.6	-82.8	-127.2	-113.4	-93.0
		2	39.9	-25.3	0.0	0.0	0.0	50.5	-32.1	0.0	0.0	0.0	62.4	-39.6	0.0	0.0	0.0
140	Flat < 2:12 (9.46 deg)	1	NA	NA	-80.2	-71.5	-58.6	NA	NA	-101.5	-90.5	-74.2	NA	NA	-125.3	-111.7	-91.6
		2	NA	NA	0.0	0.0	0.0	NA	NA	0.0	0.0	0.0	NA	NA	0.0	0.0	0.0
	3:12 (14.0 deg)	1	-78.7	-53.5	-80.2	-71.5	-58.6	-99.6	-67.7	-101.5	-90.5	-74.2	-123.0	-83.6	-125.3	-111.7	-91.6
		2	11.4	-16.0	0.0	0.0	0.0	14.4	-20.2	0.0	0.0	0.0	17.7	-24.9	0.0	0.0	0.0
	4:12 (18.4 deg)	1	-64.7	-52.2	-80.2	-71.5	-58.6	-81.9	-66.1	-101.5	-90.5	-74.2	-101.1	-81.6	-125.3	-111.7	-91.6
		2	22.4	-22.9	0.0	0.0	0.0	28.4	-29.0	0.0	0.0	0.0	35.0	-35.8	0.0	0.0	0.0
	5:12 (22.6 deg)	1	-51.9	-52.2	-80.2	-71.5	-58.6	-65.7	-66.1	-101.5	-90.5	-74.2	-81.1	-81.6	-125.3	-111.7	-91.6
		2	29.8	-25.0	0.0	0.0	0.0	37.7	-31.6	0.0	0.0	0.0	46.6	-39.0	0.0	0.0	0.0
	6:12 (26.6 deg)	1	-41.7	-52.2	-80.2	-71.5	-58.6	-52.8	-66.1	-101.5	-90.5	-74.2	-65.2	-81.6	-125.3	-111.7	-91.6
		2	32.9	-25.0	0.0	0.0	0.0	41.7	-31.6	0.0	0.0	0.0	51.4	-39.0	0.0	0.0	0.0
	9:12 (36.9 deg)	1	-24.1	-52.2	-80.2	-71.5	-58.6	-30.6	-66.1	-101.5	-90.5	-74.2	-37.7	-81.6	-125.3	-111.7	-91.6
		2	39.4	-25.0	0.0	0.0	0.0	49.8	-31.6	0.0	0.0	0.0	61.5	-39.0	0.0	0.0	0.0
	12:12 (45.0 deg)	1	-13.6	-52.2	-80.2	-71.5	-58.6	-17.2	-66.1	-101.5	-90.5	-74.2	-21.3	-81.6	-125.3	-111.7	-91.6
		2	39.4	-25.0	0.0	0.0	0.0	49.8	-31.6	0.0	0.0	0.0	61.5	-39.0	0.0	0.0	0.0
130	Flat < 2:12 (9.46 deg)	1	NA	NA	-79.0	-70.4	-57.7	NA	NA	-100.0	-89.1	-73.1	NA	NA	-123.4	-110.0	-90.2
		2	NA	NA	0.0	0.0	0.0	NA	NA	0.0	0.0	0.0	NA	NA	0.0	0.0	0.0
	3:12 (14.0 deg)	1	-77.5	-52.7	-79.0	-70.4	-57.7	-98.1	-66.7	-100.0	-89.1	-73.1	-121.1	-82.3	-123.4	-110.0	-90.2
		2	11.2	-15.7	0.0	0.0	0.0	14.1	-19.9	0.0	0.0	0.0	17.5	-24.6	0.0	0.0	0.0
	4:12 (18.4 deg)	1	-63.7	-51.4	-79.0	-70.4	-57.7	-80.6	-65.1	-100.0	-89.1	-73.1	-99.5	-80.3	-123.4	-110.0	-90.2
		2	22.1	-22.6	0.0	0.0	0.0	27.9	-28.6	0.0	0.0	0.0	34.5	-35.3	0.0	0.0	0.0
	5:12 (22.6 deg)	1	-51.1	-51.4	-79.0	-70.4	-57.7	-64.7	-65.1	-100.0	-89.1	-73.1	-79.9	-80.3	-123.4	-110.0	-90.2
		2	29.4	-24.6	0.0	0.0	0.0	37.2	-31.1	0.0	0.0	0.0	45.9	-38.4	0.0	0.0	0.0
	6:12 (26.6 deg)	1	-41.1	-51.4	-79.0	-70.4	-57.7	-52.0	-65.1	-100.0	-89.1	-73.1	-64.1	-80.3	-123.4	-110.0	-90.2
		2	32.4	-24.6	0.0	0.0	0.0	41.0	-31.1	0.0	0.0	0.0	50.6	-38.4	0.0	0.0	0.0
	9:12 (36.9 deg)	1	-23.8	-51.4	-79.0	-70.4	-57.7	-30.1	-65.1	-100.0	-89.1	-73.1	-37.1	-80.3	-123.4	-110.0	-90.2
		2	38.7	-24.6	0.0	0.0	0.0	49.0	-31.1	0.0	0.0	0.0	60.5	-38.4	0.0	0.0	0.0
	12:12 (45.0 deg)	1	-13.4	-51.4	-79.0	-70.4	-57.7	-17.0	-65.1	-100.0	-89.1	-73.1	-21.0	-80.3	-123.4	-110.0	-90.2
		2	38.7	-24.6	0.0	0.0	0.0	49.0	-31.1	0.0	0.0	0.0	60.5	-38.4	0.0	0.0	0.0

Chapter 28

28.4.3 Roof Overhangs.

The positive external pressure on the bottom surface of windward roof overhangs shall be determined using $GC_p = 0.7$ in combination with the top surface pressures determined using Fig. 28.4-1.

Fig 28.4-1

Notes:

8. For Load Case A, the roof pressure the roof pressure coefficient (GC_{pf}), when negative in Zone 2 and 2E, shall be applied in Zone 2/2E for a distance from the edge of roof equal to 0.5 times the horizontal dimension of the building ~~parallel to the direction of the MWFRS being designed~~ measured perpendicular to the ridge line or 2.5 times the eave height at the windward wall, whichever is less; the remainder of Zone 2/2E extending to the ridge line shall use the pressure coefficient (GC_{pf}) for Zone 3/3E.

Fig 28.6-1

Notes:

10. For Load Case A, the roof pressure the roof pressure coefficient (GC_{pf}), when negative in Zone 2 and 2E, shall be applied in Zone 2/2E for a distance from the edge of roof equal to 0.5 times the horizontal dimension of the building measured perpendicular to the ridge line or 2.5 times the eave height at the windward wall, whichever is less; the remainder of Zone 2/2E extending to the ridge line shall use the pressure coefficient (GC_{pf}) for Zone 3/3E.

Chapter 29

IN THE FIRST SENTENCE OF SECTION 29.5 CHANGE "h>60°" TO "h>60'".

COMMENTARY

Chapter C1

C1.3.1 Strength and Stiffness.

FIRST PARAGRAPH

Chapter ~~6~~30 of this standard specifies wind loads that must be considered in the design of cladding. Chapter 13 of this standard specifies earthquake loads and deformations that must be considered in the design of nonstructural components and systems designated in that chapter.

Chapter C2

C2.3.2 Load Combinations Including Flood Load.

DELETE THE 8TH PARAGRAPH

~~The fluid load is included in the load combinations where its effects are additive to the other loads (load combinations 1 through 5). Where F acts as a resistance to uplift forces, it should be included with dead load D. The mass of the fluid is included in the inertial effect due to E (see 15.4.3) and the base shear calculations for tanks (15.7). To make it clear that the fluid weight in a tank can be used to resist uplift, F was added to load combination 7 where it will be treated as dead load only when F counteracts E. Note that the fluid mass effects on stabilization depend on the degree to which the tank is filled. F is not included in combination 6 because the wind load can be present, whether the tank is full or empty, so the governing load case in combination 6 is when F is zero.~~

C2.3.4 Load Combinations Including Atmospheric Ice Loads.

Load combinations ~~1 and 2~~ (2), (4), and (6) in Section~~s~~ 2.3.4 and load combinations (2), (3) and (7) in Section 2.4.3 include the simultaneous effects of snow loads as defined in Chapter 7 and Atmospheric Ice Loads as defined in Chapter 10.

Chapter C7

C7.2 GROUND SNOW LOADS, p_g

AT THE END OF THE 4TH TO LAST PARAGRAPH CHANGE:

For example, a ground snow load based on a 3.3% annual probability of being exceeded (30-yr mean recurrence interval) should be multiplied by 1.18 to generate a value of p_g for use in Eq. ~~7-1~~7.3-1.

C7.7 DRIFTS ON LOWER ROOFS (AERODYNAMIC SHADE)

REVISE END OF 4TH TO LAST PARAGRAPH AND INSERT NEW PARAGRAPH BELOW.

The drift load provisions cover most, but not all, situations. Finney (1939) and O'Rourke (1989) document a larger drift than would have been expected based on the length of the upper roof. The larger drift was caused when snow on a somewhat lower roof, upwind of the upper roof, formed a drift between those two roofs allowing snow from the upwind lower roof to be carried up onto the upper roof then into the drift on its downwind side. It was suggested that the sum of the lengths of both roofs could be used to calculate the size of the leeward drift. ~~The issue of potential reduction in leeward drift size at a roof step due to a parapet wall is discussed in O'Rourke (2007).~~

Generally, the addition of a parapet wall on a high roof cannot be relied upon to substantially reduce the leeward snow drift loading on an adjacent or adjoining lower roof. This is particularly true for the case of a single parapet wall of typical height located at the roof step. Also, the addition of a parapet wall at a roof step would increase the space available for windward drift formation on the lower roof. The issue of potential reduction in leeward drift size at a roof step due to a parapet wall is discussed in more detail in O'Rourke (2007).

C7.8 ROOF PROJECTIONS AND PARAPETS

NEW PARAGRAPH AT THE END OF THE SECTION.

Refer to Section C7.7 for more description of the effects that a parapet wall at a high roof can have on the snow drift loading at an adjacent or adjoining lower roof.

C7.13 OTHER ROOFS AND SITES

Example 2

CHANGE "*I*" TO "I_s" IN 2 LOCATIONS. CHANGE THE "Tangent of the vertical angle from eaves to crown" FROM "= 5/40" TO "= 15/40"

…

Flat-Roof Snow Load:

$$p_f = 0.7 C_e C_t I_s p_g$$

where

p_g = 25 lb/ft^2 (1.20 kN/m^2) (from Fig. 7-1)
C_e = 0.9 (from Table 7-2 for Terrain Category B and a fully exposed roof)
C_t = 1.0 (from Table 7-3)
I_s = 1.1 (from Table 1.5-2)

Thus:

p_f = (0.7)(0.9)(1.0)(1.1)(25) = 17 lb/ft^2
In SI: p_f = (0.7)(0.9)(1.0)(1.1)(1.19) = 0.83 kN/m^2
Tangent of vertical angle from eaves to crown = 15/40 = 0.375
Angle = 21°.
Because the vertical angle exceeds 10°, the minimum roof snow load, p_m, does not apply. See Section 7.3.4.

Example 3

CHANGE "*I*" TO "I_s" IN 4 LOCATIONS.

…

High Roof:

$$p_f = 0.7 C_e C_t I_s p_g$$

where

p_g = 40 lb/ft^2 (1.92 kN/m^2) (given)
C_e = 0.9 (from Table 7-2)
C_t = 1.0 (from Table 7-3)
I_s = 1.1 (from Table 1.5-2)
…

Low Roof:

$$p_f = 0.7 C_e C_t I_s p_g$$

where

p_g = 40 lb/ft^2 (1.92 kN/m^2) (given)
C_e = 1.0 (from Table 7-2) partially exposed due to presence of high roof
C_t = 1.0 (from Table 7-3)
I_s = 0.8 (from Table 1.5-2)



Figure 22-7 Maximum Considered Earthquake Geometric Mean (MCE_G) PGA, %g, Site Class B for the Conterminous United States.

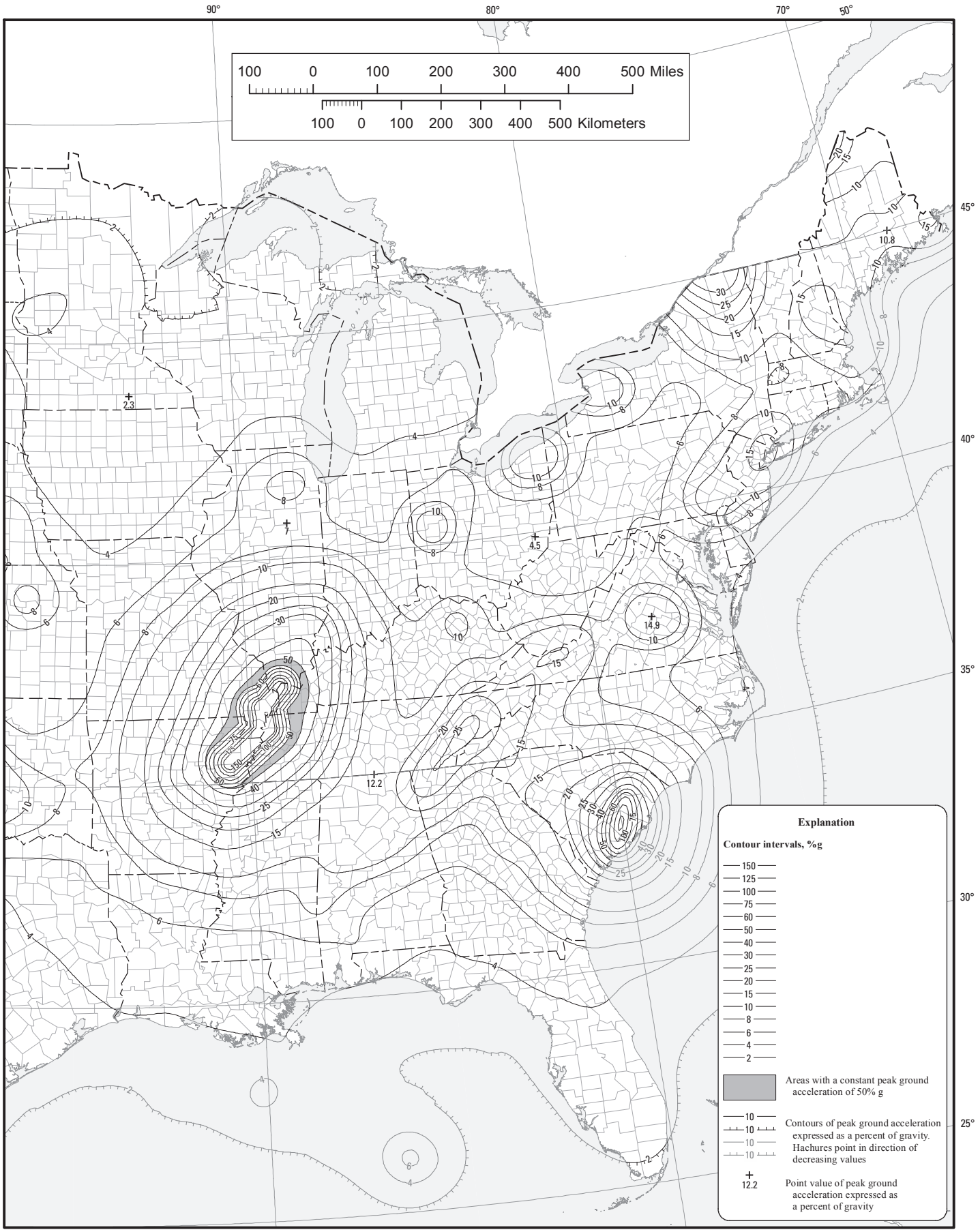


Figure 22-7 (*continued*) Maximum Considered Earthquake Geometric Mean (MCE_G) PGA, %g, Site Class B for the Conterminous United States.

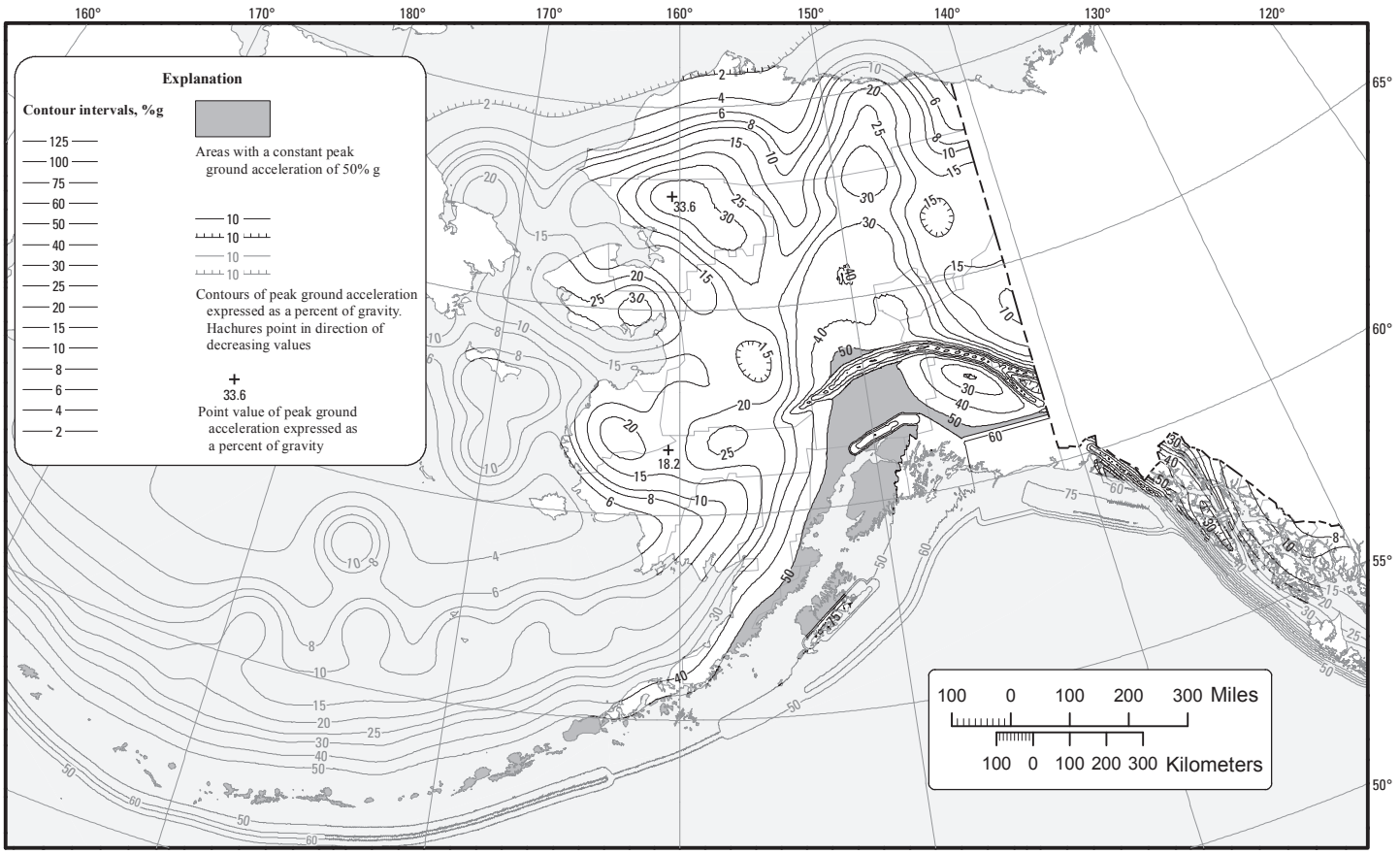


Figure 22-8 Maximum Considered Earthquake Geometric Mean (MCE_G) PGA, %g, Site Class B for Alaska.

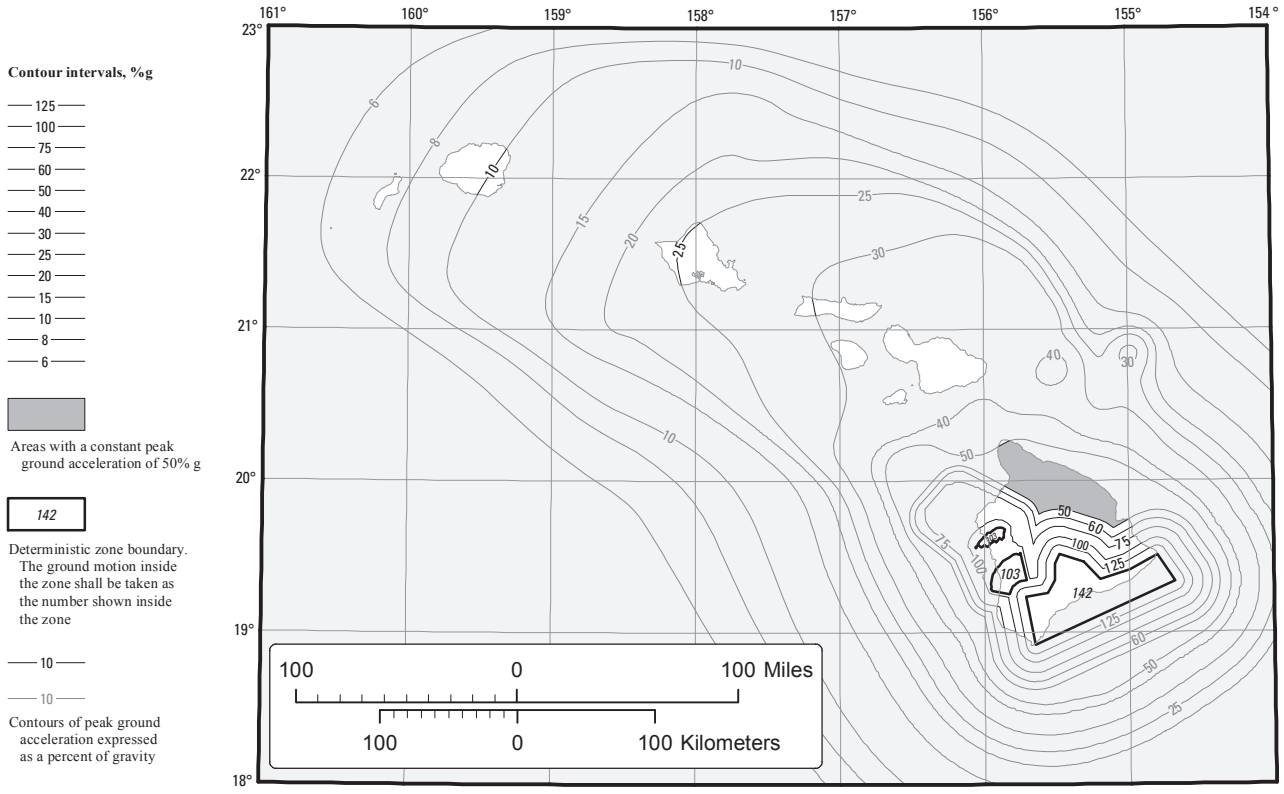


Figure 22-9 Maximum Considered Earthquake Geometric Mean (MCE_G) PGA, %g, Site Class B for Hawaii.