

0							
0	DI	ESIGN CRITE	RIA	CODE :	IBC 2006		Sht. DS1
ROOF LOAD DURATION = SNOW LOADING ?	1.25 LDF NO						
PITCHED ROOF ROOF DL = ROOF LL =	R1 22.5 PSF 20 PSF	R1 R PITCH R	OOF PITCH = EDUCTION =	5.0:12 0.95			
FLAT ROOF ROOF DL = ROOF LL =	R2	R2 R PITCH R	OOF PITCH = EDUCTION =	0.3:12 1.00	FLAT ROOF ROOF DL = ROOF LL =	R3 12 PSF 12 PSF	
FLOOR DL = FLOOR LL =	F1		OPEN LA JOIST/RAFTI JOIST/RAFTI	ATTICE DL = ER WIDTH = ER DEPTH = SPACING =			
DECK DL = DECK LL =	F2		STAIR DL = STAIR LL =	F3			-
LATERAL: WIND GOVERNS? WIND VELOCITY = WIND EXPOSURE :	YES 90 MPH C	3-SEC GUST					
SAWN LUMBER: SPECIES AN 2 x 6 : 2 x - 4 x THICK (2 X 8 etc): 6 x AND THICKER : 2 x 4 STUDS : 2 x 4 STUDS : 2 x 6 STUDS : 2 x 6 STUDS : SPECIAL (SEE CALCS) SPECIAL (SEE CALCS) 2 x AND 3 x MUD SILL : GLULAM BEAMS : DF/DF GLULAM COLUMNS : DF/DF RESID. PARALLAM BEAMS : PARALLAM COLUMNS :	D GRADES L HEM-FIR DF-L HEM-FIR HEM-FIR HEM-FIR DF-L GLB C&C GLB GLC PSL Com PSL PSL Col	LISTED ARE M # 2 # 1 Stud # 2 Stud # 2 24F-V4 24F-V4 24F-V8 Comb 2 DF 2.0E 2.2E 1.8E	INIMUM. BETTE (LEDGERS, BE (LEDGERS, 4 : (POSTS, BEAN WALL HEIGHT WALL HEIGHT WALL HEIGHT WALL HEIGHT 2 x TO 4 x 6 x AND THICH FOR SIMPLE S FOR CONTINU 9.25" TO 18" D 20" AND GREA 3.5" TO 7" DIM	ER MAY BE S EAMS, AND H X POSTS, BE. MS, AND HEA S UP TO TS MORE TH/ S UP TO TS MORE TH/ SPANS (STD JOUS AND C. EEP ATER DEPTH ENSIONS	UBSTITUTED IEADERS) AMS, AND HE DERS) 8'-1" AN 8'-1" 10'-1" AN 10'-1" CAMBER U.N ANTILEVERS	ADERS) NOTE: POST AND TR SPECIES/GRA ON WALL HEIG ACTUAL POST W/ INCISED J.O.)	IMMER DE BASED GHT, NOT /TRIM HT.
PRE-FAB TRUSSES: TO BE EN DRAWINGS AND CALCULATIO	GINEERED NS SEALED	BY TRUSS MA BY ARIZONA	NUFACTURER REGISTERED I	WITH SHOP ENGINEER.			

CONVENTIONAL FOUNDATIONS: SOIL BEARING PRESSURE = 1500 PSF CONCRETE 28-DAY F'c = 2500 PSI POST-TENSIONED FOUNDATIONS: SOIL BEARING PRESSURE = 1250 PSF POST-TENSION CONCRETE 28-DAY F'c = 2500 PSI

LOAD CODE DEAD TL R2 x I IVF (See Design ROOF R1 22 19 41 psf Specs sheet preceeding this ROOF R3 12 12 24 psf sheet) Note: "R" or "F" Load Codes are used to determine load combination allowable stresses. LOAD CODE TRIB 1 OR ENTIRE SPAN TRIB 2 TRIB 3 TRIB 4 (CANTILEVER) F1 5 (FT) R1 7 (FT) R2 8 (FT) 12 (FT) Additional Dead or Total Load Example: TL = (55 x 5) + (38 x 7) = 541 PLF D/TL D/TL 28 PLF 42 PLF 28 PLF 541 PLF 280 PLF 420 PLF Coded TL Length 4 FT 3 FT 6 FT OVERALL L = 13 FT LEFT OR "SOUTH" NO. TRIMMER STUDS REQ'D MOMENT = 9185 FT-LBS TL DEFL= 0.33" LOCATION OF MAX. M = 6.6' 1404 LBS=GOVERN'G SHEAF END OF MEMBER @ LDF = 1.25 BRG L = 1.13" LL DEFL= 0.14" BRG L =1.03" STRESS RATIOS DROP/RAISED NO. OF PLIES 1917 DURATION SPECIES GRADE 1404 SHEAR=0.79 988/677 1.25 LDF 3 pcs 1380/123 MOMENT=0.90 Camber OK? R=3184 LBS Try 2 x 12 BEAM REP R=2907 LBS TL DEFL.= L/477 NO. PCS SIZE SPECIES GRADE REP ? REC'M'D = L/320 BEAM LABEL DF-L 3 2 x 12 #2 Yes ROOF LIVE = 1380 LBS BACK-OFF "d" FOR SHEAR AT : FLOOR LIVE = 123 LBS ALL BEAMS/HEADERS ? NO CHECK CURRENT DESIGN : "TAG" SIMILAR BEAMS ? NO ALL BEAMS/HEADERS DEEPER THAN 15" ? YES If same size or more: PREVIOUS MARK SPAN >=, LOAD >= ? YES ADD DEAD LOAD TO ALL HEADERS = 20 PLF If same size or less: PREVIOUS MARK SPAN <=, LOAD <= ? YES ADD SELF-LOAD TO HEADERS / BEAMS : YES LOAD ECCENTRICITY = d / 6 FOR POSTS/TRIMMERS ? YES **REDUCE ROOF LIVE ?** YES **REDUCE FLOOR LIVE ?** YES LOAD CASE ( D + 0.75 x Lr (or S) + 0.75 x L ) ? YES HDR TRIM HEIGHT FLAT ROOF HEADER TRIM HT (R3 ONLY) = FIRST FLR CLG HEIGHT = 10. FT 7.5 FT FLAT ROOF TOP OF PARAPET (R3 ONLY) = SECOND FLR CLG HEIGHT = THIRD FLR CLG HEIGHT = ADD DEAD LOAD TO FLAT ROOF HDRS (R3 ONLY) = 0 PLF FOURTH FLR CLG HEIGHT =

LOAD CRITERIA AND EXAMPLE OF HEADER/BEAM DESIGN OUTPUT

"FLAT ROOF" SLOPE = > 1/4 IN./FT. ? YES

NOTES:

FLOOR HEIGHT =

- 1) When both floor and roof live loads are applied, allowable bending and shear stresses are multiplied by LDF = 1.25. The load case with floor live load only is also checked, using LDF = 1.00
- 2) Dead load only case is automatically checked with LDF = 0.90
- 3) Dropped beams or headers are automatically checked for Stability Factor, and allowable bending stress is reduced accordingly.
- 4) Glulam beams are automatically checked for Volume Factor, and allowable bending stress is reduced accordingly. If Stability Factor (dropped beams and headers only) is less than Volume Factor, it governs bending stress reduction. Camber is checked for spans in excess of 8'
- 5) Floor live loads reduced per IBC Sect. 1607.9.2; Roof live loads reduced per IBC Sect. 1607.11.2
- 6) Post design is based on ceiling (wall top plate) height, with depth of supported beam deducted.
- 7) For cantilever, check beam design with live load on cantilever only.

Sht. DS2

## CONTINUOUS ELEMENTS AND ADDITIONAL NOTES

When continuous trusses, girder trusses, and beams are analyzed in this calculation set, each span designated with the trailing alphabetic identifier A, B, C, etc., starting at the left (south) end.

Example of 3-span continuous member :



On the framing plan(s), this would be called out as a single member, for example GT5 (4-pt brg), because no additional info is necessary for construction and to reduce complexity of the drawings.



## ALSO:

When girder trusses, headers and beams above the second floor are analyzed in this calculation set, they are prefixed with the letter R. Example: RGT3, RB5. The "R" prefix is not used on the drawings.

When girder trusses, headers and beams above the first floor are analyzed in this calculation set, they are prefixed with the number 2. Example: 2GT9, 2B16. The "2" prefix is not used on the drawings. There also will be some RB- headers that









DESIGN OF STUDS, POSTS, TRIMMERS, KING STUDS



Sht. S1



0								Sht. CF-1
		FO	UNDATI	ON DESIG	N			
ALLC	DW SOIL BRG I	PRESSURE = 1	500. psf	ALI	OW BASEME	NT SOIL BRG	PRESSURE =	2000. psf
CONTINUOUS	FOOTING DE	SIGNS: ALL 10" TH	HICK UNLE	ESS NOTED C	OTHERWISE.			
	WT1	WT2	WT3	WT4	WT5	WT6	WT7	WT8
RF LOAD =	:							
FLR LOAD =	:							
STUD WALL =	:							
BSMT/MISC.=								
IOTAL =								
W REQ'D =								
USE FIG :								
					ISE			
Eor unoqual bo	am reactions of	uffix "I" "M' or "P	LOO NOT	is "I " reaction	noL.			Post Dosign?
SF2	ann reactions, s	ΔCTLIA			Π by default. ΜΔ x			FOSt Design?
012			PACITY -	6000 lbs				
		REQ'	D AREA =	0.00 ft.^2				
	NOT USED	SIZE OF SQUA	RE FTG =	0.0 in.				
		0.22 01 0000		010				
								Post Design?
SF2.5		ACTUA	L LOAD =	8265 lbs	MAX	LOAD FROM	GT1AL	
		LOAD CA	PACITY =	9375 lbs		ALSO FROM		
		REQ'	D AREA =	5.51 ft.^2				
		SIZE OF SQUA	RE FTG =	28.2 in.				
	PROVIDE 30	) INCH SQUARE	FOOTIN	G	12 INCH TH	IICK W/ 3-#	4 BOTT E.V	V.
								Post Design?
<u>SF3</u>		ACTUA	L LOAD =	lbs	MAX	LOAD FROM		
		LOAD CA	PACITY =	13500 lbs		ALSO FROM		
		REQ'	D AREA =	0.00 ft.^2				
	NOT USED	SIZE OF SQUA	RE FTG =	0.0 in.				
0505								Post Design?
<u>SF3.5</u>		ACTUA	L LOAD =	15692 lbs	MAX		GT1AM	
		LOAD CA	PACITY =	18375 lbs		ALSO FROM		
				10.46 ft.^2				
		SIZE OF SQUA	REFIG=	38.8 m.				
				c				v
	FROVIDE 42			9		IIGR W/ J-#		Poot Design?
054				lle e				Post Design?
<u>3F4</u>					MAX			
				24000 IDS		ALSO FROM		
	NOT USED			0.00 it. 2				
				0.0 111.				
								Post Design?
SF4.5		ACTUA	L LOAD =	lbs	МАХ			. cor Dooigin
<u>v</u>		LOAD CA	PACITY =	30375 lbs		ALSO FROM		L
		REQ'	D AREA =	0.00 ft.^2				
	NOT USED	SIZE OF SQUA	RE FTG =	0.0 in.				

Sheet: L 1

WALL	SHEAR WALL MATERIAL SCHEDULE	ALLOWABLE <u>SHEAR</u>
SW1	7/8" 3-Coat Stucco w/ #16 Ga. Staples w/ 7/8" legs @ 6" o.c.	180 plf
SW2	1/2" Gypboard wall (unblocked) w/ 5d cooler nails 7" o.c. at edges and field.	100 plf
SW3	1/2" Gypboard wall (unblocked) w/ 5d cooler nails 4" o.c. at edges and field.	125 plf
SW4	1/2" Gypboard wall (blocked) w/ 5d cooler nails 4" o.c. at edges and field.	150 plf
SW5	5/8" Gypboard wall (unblocked) w/ 6d cooler nails 7" o.c. at edges and field.	115 plf
SW6	5/8" Gypboard wall (unblocked) w/ 6d cooler nails 4" o.c. at edges and field.	145 plf
SW7	5/8" Gypboard wall (blocked) w/ 6d cooler nails 4" o.c. at edges and field.	175 plf
SW8	Two layers of 5/8" Gypboard (blocked) w/ 6d cooler nails 9" o.c. at base ply and 8d cooler nails 7" o.c. at face ply	250 plf
SW9	3/8" blocked CDX sheathing w/ 8d common nails 6" o.c. at edges and 12" o.c. field.	220 plf
SW10	3/8" blocked CDX sheathing w/ 8d common nails 4" o.c. at edges and 12" o.c. field.	320 plf
SW11	3/8" blocked CDX sheathing w/ 8d common nails 3" o.c. at edges and 12" o.c. field.	410 plf
SW12	3/8" blocked CDX sheathing w/ 8d common nails 2" o.c. at edges and 12" o.c. field.	530 plf
SW13	15/32" blocked CDX sheathing w/ 10d common nails 6" o.c. at edges and 12" o.c. field.	260 plf
SW14	15/32" blocked CDX sheathing w/ 10d common nails 4" o.c. at edges and 12" o.c. field.	390 plf
SW15	15/32" blocked CDX sheathing w/ 10d common nails 3" o.c. at edges and 12" o.c. field.	510 plf

 0.00 0

Sheet: L 2

STRAP	<u>TYPE</u>	ALLOW. (lbs)	HOLDOWN	<u>TYPE</u>	<u>ALLOW.</u> (lbs)	
CMST14	А	5517	HD10A	Н	8045 (Triple 2x	()
2CS16	В	2899	HDU8	I.	5665	
2CS18	С	2329	PHD6/STHD <sup>7</sup>	J	8505	
2CS20	D	1751	PHD5/STHD <sup>7</sup>	K	5665	
CS16	Е	1449	PHD2/STHD <sup>7</sup>	L	1690	
CS18	F	1165	PHD2/STHD	М	3115	
CS20	G	876				

6 x 4 Post 8 x 4 Post

## ASED ON C

Note: 2CS20 denotes double CS20 strap. 2SW2 denotes SW2 applied both sides of the wall.

SHEARWALL CRITERIA

LSTHD8C, STHD10E, STHD14E denote reduced design capacity at corner or end condition where hold down is 1.5" from corner or end; actual holdowns are LSTHD8, STHD10, STHD14 etc.

LSTHD8R is reduced capacity LSTHD8 with 10-16d sinker nails. It can used as a direct replacement for the discontinued PAHD42.



Note:

Height to width ratio of all wall piers shall be 3.5:1. Entire panel is sheathed with shear mat'l, including above and below window openings. Shear panel type is determined by the "amplified" shear value q'. With this method, it is not necessary to design for force transfer around openings, and straps are typically not required at the opening corners.

With multi-panel shearwalls, value of q' = \_\_\_\_\_ Total P

0.00									
0								Sheet: L	3
-		W	IND PRE	SSURE W	ORKSHE	ET			-
WIND	n – a v G		vlt Wind	l Spood V -	90 mph	Exposure :	C	Roof <b>n</b> . –	0.0 pef
	$p = q \times G$		YSTEM	Fff $A_{v} =$	s f		1.00	h = h - h	16.6'
Walls		Windward	Leeward	G =	0.85	WR1 Pitch=	5.0.12	- 11	n2 R
<u>wano</u>	Kz	<b>p</b> <sub>7</sub> (psf)	<b>p</b> <sub>h</sub> (psf)	Kh =	0.90	LR1 Pitch=	5.0:12	Use :	p2_N p2_LW
p1 (0'-15')	0.85	11.6	7.2	Cp =	1.3	Windward a	nd Leeward	Walls (p W)	)
p2 (15' - 20')	0.90	12.3	7.7	Cp =	0.8	Windward W	/all (p WW	)	
p3 (20' - 25' )	0.94	12.8	8.0	Cp =	0.5	Leeward Wa	all (p_LW)	, ,	
,				Cp =	0.23	Windward R	oof (p_WR)		
				Cp =	0.60	Leeward Ro	of (p_LR)		
				Cp =	0.83	Windward a	nd Leeward	Roofs (p_R)	
p3	Max.=	23.1'			Numbe	r of Stories =	1		
	φ								
p2 ↔					Shear P	anel Label =	SW		
$\Box$ .									
p1 ↔					WR Pi	tch Length =	31.5'		
	H =	10.0'			LR Pi	tch Length =	31.5'		
WIND FRON	T/BACK	Total \	Wind (lbs) =	0	< < GOVE	RNS FRONT	/ BACK		
ROO	F	Wa	II Subtotal =	0			Roc	of Subtotal =	0
Wall:	Length	Height	Pressure	Wind Load	Roof :	Length	Ht / Width	Pressure	Wind Load
WIND LEFT	/RIGHT	Total \	Wind (lbs) =	0	< < GOVE	RNS LEFT /	RIGHT		-
ROO	F	Wa	II Subtotal =	0			Roc	of Subtotal =	0
Wall:	Length	Height	Pressure	Wind Load	Roof :	Length	Ht / Width	Pressure	Wind Load
		ļ							
		ļ	ļ						
				•		•			



0.00								
0		SHEAF	RWALL AN	ALYSIS			Sheet: L	
Panel Mark :								
$\Sigma$ Lateral P =								
Load Type (W, EQ) :								
At Elevated Floor ?								
L(ft.) =								
П ( IL.) = АРА ТР157 Агез* –								
Perforated Length* =								
Shearwall F =								
q ( plf ) =								
L' <sub>total</sub> =								
q' ( plf ) =								
Select Shearwall :								
		ļ	ļ	Į	1		Į	ļ
Panel Mark (above) :								
q (above) =	0	0	0	0	0	0	0	0
H (above - ft.) =	0	0	0	0	0	0	0	0
Panel Above L (ft.) =	0	0	0	0	0	0	0	0
Unset - from LH end = $\lfloor$								
→ Dir R M <sub>OT</sub> (ft-lbs) =								
$\bullet  \text{Dir L } M_{OT} ( \text{ ft-lbs } ) =$								
Unif. W <sub>D</sub> ( plf ) =								
Panel Above Unif. W <sub>D</sub> ( plf ) =								
Dist. 1 ( ft.) =								
Dist. 2 ( ft.) =								
Dist. 3 (ft.) =								
Part. $W_{D1}$ (pif) = Part $W_{C1}$ (pif) =								
Part $W_{D2}$ (plf) =								
$(LH) P_{D1} (lbs) =$								
$P_{D2}$ (lbs) =								
$P_{D3}$ ( lbs) =								
(RH) P <sub>D4</sub> ( lbs) =								
Dir. R $M_R$ (ft-lbs) =								
Dir. L $M_R$ (ft-lbs) =								
Dir. R M <sub>NET</sub> (ft-lbs) =								
Dir. L $M_{NET}$ (ft-lbs) =								
H and I plift ( lbs ) -								
RH end Unlift ( lbs ) =								
-				-		1		
LH end Holdown :								
RH end Holdown :								
1 H and Stude/Dact -								
BH end Studs/Post :								
<b>8d</b> or 0.138 in dia shotnin =								
$(At L_{EFF})$ 16d toenails =								
Directly over shear wall								
$2 \times 6$ blocking o/c =								
Simpson LTP4 $o/c =$								
Simpson A35, A35F o/c =								
At L <sub>EFF</sub> ( ft.) =								
2 x 6 blocking o/c =								
Simpson LTP4 o/c =								
Simpson A35, A35F o/c = _		1	1	1	1	1	1	1
		1	1	1	1	1	1	1

0.00 0 SHEARWALL ANALYSIS Sheet: L Panel Mark :  $\Sigma$  Lateral P = Load Type (W, EQ): At Elevated Floor ? L ( ft.) = H ( ft.) = APA TR157 Area\* = Perforated Length\* = Shearwall F = q ( plf ) = L'<sub>TOTAL</sub> = q' ( plf ) = H/L =Allowed Types : Select Shearwall : Panel Mark (above) : 0 q (above) = 0 0 0 0 0 0 0 H (above - ft.) = 0 0 0 0 0 0 0 0 Panel Above L ( ft.) = 0 0 0 0 0 0 0 0 Offset - from LH end = Dir R  $M_{OT}$  (ft-lbs) = Dir L M<sub>OT</sub> (ft-lbs) = Unif.  $W_D$  ( plf ) = Panel Above Unif. W<sub>D</sub> ( plf ) = Dist. 1 ( ft.) = Dist. 2 ( ft.) = Dist. 3 ( ft.) = Part. W<sub>D1</sub> (plf) = Part. W<sub>D2</sub> ( plf ) = Part.  $W_{D3}$  ( plf ) = (LH) P<sub>D1</sub> ( lbs) =  $P_{D2}$  (lbs) =  $P_{D3}$  (lbs) = (RH) P<sub>D4</sub> ( lbs) = Dir. R  $M_R$  (ft-lbs) = Dir. L  $M_R$  (ft-lbs) = Dir. R M<sub>NET</sub> (ft-lbs) = Dir. L M<sub>NET</sub> (ft-lbs) = LH end Uplift ( lbs ) = RH end Uplift ( lbs ) = LH end Holdown : RH end Holdown : LH end Studs/Post : RH end Studs/Post : 16d or 1/2 in. dia. a.b. o/c = 8d or 0.138 in. dia. shotpin = (At L<sub>EFF</sub>) 16d toenails = Directly over shear wall 2 x 6 blocking o/c = Simpson LTP4 o/c = Simpson A35, A35F o/c = At  $L_{EFF}$  (ft.) = 2 x 6 blocking o/c = Simpson LTP4 o/c = Simpson A35, A35F o/c =

0.00							-	
0		MU	JLTIPANEL	SHEARWA	LL ANALYS	SIS	Sheet: L	
		Elev. Floor?		L <sub>TOT</sub> =	0.0 ft.	a =	0. plf	
Load Type (W, EQ):		(L, R, Both)?	Both	L' <sub>TOT</sub> =	0.0 ft.	q' =	0. plf	
Ht. (ft.) =								
L ( ft.) =								1
H ( ft.) =								
APA TR157 Area* =								
Perforated Length* =								
H/L =								
Allowed Types :								
Select Shearwall :								
								1
Panel Mark (above) :	0	0	0	0	0	0	0	
q (above) = H (above - ft ) =	0	0	0	0	0	0	0	0
Panel Above L ( ft.) =	0	0	0	0	0	0	0	0
Offset - from LH end =	-	-	-	-	-	-	-	-
Q(lbs)= Dir R M <sub>OT</sub> (ft-lbs)=								
Dir L $M_{OT}$ (ft-lbs) =								
Unif. $W_D$ (plf) =								
Panel Above Unit: $W_D(pil) =$ Dist 1(ft) -								
Dist. 2 ( ft.) =								
Dist. 3 ( ft.) =								
Part. $W_{D1}$ (plf) =								
Part. $W_{D2}$ (plf) =								
$(LH) P_{D1} (lbs) =$								
$P_{D2}$ (lbs) =								
$P_{D3}$ ( lbs) =								
(RH) P <sub>D4</sub> ( lbs) =								
Dir. R $M_R$ (ft-lbs) =								
Dir. L $M_R$ (ft-lbs) =								
Dir. R M <sub>NET</sub> (ft-lbs) =	0							
DII. L $M_{NET}$ (II-IDS) =	0							
LH end Uplift ( lbs ) =	0							
RH end Uplift ( lbs ) =	0							
LH end Holdown :								
KH end Holdown.								
I H end Studs/Post ·								
RH end Studs/Post :								
Shear T	ransfer			Directly or	ver shear wall	At L <sub>EFF</sub> =		]
1/2 in. dia. a.b. o/c =			2 x 6	blocking o/c =				
0.138 in. dia. shotpin =			Simpson A	on LTP4 o/c = $\frac{1}{25}$				
$(\neg L = EFF)$ for toenalis =			Simpson Ad	55, ASSE 0/C =				

0.00								-	
0			М	JLTIPANEL	SHEARWA	LL ANALYS	SIS	Sheet: L	
			Elev. Floor?		L <sub>TOT</sub> =	0.0 ft.	a =	0. plf	
Load T	ype (W, EQ):		(L, R, Both)?	Both	L' <sub>TOT</sub> =	0.0 ft.	q' =	0. plf	
Ht. ( ft.) =					-				
	L ( ft.) =								
	H ( ft.) =								
APA TR157	Area* =								
Perforated	Lengtn <sup>*</sup> =								
Shearwan	' -L H/L =								
Allo	owed Types :								
Selec	t Shearwall :								
	. r								
Panel M	ark (above) :	0	0	0	0	0	0	0	0
н	q (above) = (above) = (above - ft) = (above - ft)	0	0	0	0	0	0	0	0
Panel Al	bove L (ft.) =	0	0	0	0	0	0	0	0
Offset - fr	om LH end =								
Dir R M Dir L M Uni Panel Above Uni Pant Part Part	$Q (lbs) = M_{OT} (ft-lbs) = M_{OT} (ft-lbs) = f. W_D (plf) = f. W_D (plf) = Dist. 1 (ft.) = Dist. 2 (ft.) = Dist. 3 (ft.) = . W_{D1} (plf) = . W_{D2} (plf) = . W_{D2} (plf) = . W_{D3} (plf) =$								
(RH	$P_{D2}$ (lbs) = $P_{D3}$ (lbs) =								
Dir. R Dir. L Dir. R M Dir. L M LH end	$M_{R} (ft-lbs) =$ $M_{R} (ft-lbs) =$ $M_{R} (ft-lbs) =$ $M_{RT} (ft-lbs) =$ $M_{RT} (ft-lbs) =$ $M_{RT} (ft-lbs) =$ $M_{RT} (ft-lbs) =$	0 0							
LH e	nd Holdown :	0							
			1		1			1	
LH end RH end 1/2 in. c 0.138 in. c (At L <sub>EFF</sub> ) 1	Studs/Post : Studs/Post : <u>Shear T</u> dia. a.b. o/c = dia. shotpin = 6d toenails =	ransfer		2 x 6 Simps Simpson A3	Directly or blocking o/c = on LTP4 o/c = 35, A35F o/c =	ver shear wall	At L <sub>EFF</sub> =		]
	]								

0.00								-	
0			М	JLTIPANEL	SHEARWA	LL ANALYS	SIS	Sheet: L	
			Elev. Floor?		L <sub>TOT</sub> =	0.0 ft.	a =	0. plf	
Load T	ype (W, EQ):		(L, R, Both)?	Both	L' <sub>TOT</sub> =	0.0 ft.	q' =	0. plf	
Ht. ( ft.) =					-				
	L ( ft.) =								
	H ( ft.) =								
APA TR157	Area* =								
Perforated	Lengtn <sup>*</sup> =								
Offeatwall	' -L H/L =								
Allo	owed Types :								
Selec	t Shearwall :								
	. r								
Panel M	ark (above) :	0	0	0	0	0	0	0	0
н	q (above) = (above) = (above - ft) = (above - ft)	0	0	0	0	0	0	0	0
Panel Al	bove L ( ft.) =	0	0	0	0	0	0	0	0
Offset - fr	om LH end =								
Dir R M Dir L M Uni Panel Above Uni Pant Part Part	$Q (lbs) = M_{OT} (ft-lbs) = M_{OT} (ft-lbs) = f. W_D (plf) = f. W_D (plf) = Dist. 1 (ft.) = Dist. 2 (ft.) = Dist. 3 (ft.) = . W_{D1} (plf) = . W_{D2} (plf) = . W_{D2} (plf) = . W_{D3} (plf) =$								
(RH	$P_{D2}$ (lbs) = $P_{D3}$ (lbs) =								
Dir. R Dir. L Dir. R M Dir. L M LH end	$M_{R} (ft-lbs) =$ $M_{R} (ft-lbs) =$ $M_{R} (ft-lbs) =$ $M_{RT} (ft-lbs) =$ $M_{RT} (ft-lbs) =$ $M_{RT} (ft-lbs) =$ $M_{RT} (ft-lbs) =$	0 0							
LH e	nd Holdown :	0							
			1		1			1	
LH end RH end 1/2 in. c 0.138 in. c (At L <sub>EFF</sub> ) 1	Studs/Post : Studs/Post : <u>Shear T</u> dia. a.b. o/c = dia. shotpin = 6d toenails =	ransfer		2 x 6 Simps Simpson A3	Directly or blocking o/c = on LTP4 o/c = 35, A35F o/c =	ver shear wall	At L <sub>EFF</sub> =		]
	]								

0.00								-	
0			М	JLTIPANEL	SHEARWA	LL ANALYS	SIS	Sheet: L	
			Elev. Floor?		L <sub>TOT</sub> =	0.0 ft.	a =	0. plf	
Load T	ype (W, EQ):		(L, R, Both)?	Both	L' <sub>TOT</sub> =	0.0 ft.	q' =	0. plf	
Ht. ( ft.) =					-				
	L ( ft.) =								
	H ( ft.) =								
APA TR157	Area* =								
Perforated	Lengtn <sup>*</sup> =								
Shearwan	' -L H/L =								
Allo	owed Types :								
Selec	t Shearwall :								
	. r								
Panel M	ark (above) :	0	0	0	0	0	0	0	0
н	q (above) = (above) = (above - ft) = (above - ft)	0	0	0	0	0	0	0	0
Panel Al	bove L ( ft.) =	0	0	0	0	0	0	0	0
Offset - fr	om LH end =								
Dir R M Dir L M Uni Panel Above Uni Pant Part Part	$Q (lbs) = M_{OT} (ft-lbs) = M_{OT} (ft-lbs) = f. W_D (plf) = f. W_D (plf) = Dist. 1 (ft.) = Dist. 2 (ft.) = Dist. 3 (ft.) = . W_{D1} (plf) = . W_{D2} (plf) = . W_{D2} (plf) = . W_{D3} (plf) =$								
(RH	$P_{D2}$ (lbs) = $P_{D3}$ (lbs) =								
Dir. R Dir. L Dir. R M Dir. L M LH end	$M_{R} (ft-lbs) =$ $M_{R} (ft-lbs) =$ $M_{R} (ft-lbs) =$ $M_{RT} (ft-lbs) =$ $M_{RT} (ft-lbs) =$ $M_{RT} (ft-lbs) =$ $M_{RT} (ft-lbs) =$	0 0							
LH e	nd Holdown :	0							
			1		1			1	
LH end RH end 1/2 in. c 0.138 in. c (At L <sub>EFF</sub> ) 1	Studs/Post : Studs/Post : <u>Shear T</u> dia. a.b. o/c = dia. shotpin = 6d toenails =	ransfer		2 x 6 Simps Simpson A3	Directly or blocking o/c = on LTP4 o/c = 35, A35F o/c =	ver shear wall	At L <sub>EFF</sub> =		]
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0.00								-	
0			М	JLTIPANEL	SHEARWA	LL ANALYS	SIS	Sheet: L	
			Elev. Floor?		L <sub>TOT</sub> =	0.0 ft.	a =	0. plf	
Load T	ype (W, EQ):		(L, R, Both)?	Both	L' <sub>TOT</sub> =	0.0 ft.	q' =	0. plf	
Ht. ( ft.) =					-				
	L ( ft.) =								
	H ( ft.) =								
APA TR157	Area* =								
Perforated	Lengtn <sup>*</sup> =								
Offeatwall	' -L H/L =								
Allo	owed Types :								
Selec	t Shearwall :								
	. r								
Panel M	ark (above) :	0	0	0	0	0	0	0	0
н	q (above) = (above) = (above - ft) = (above - ft)	0	0	0	0	0	0	0	0
Panel Al	bove L ( ft.) =	0	0	0	0	0	0	0	0
Offset - fr	om LH end =								
Dir R M Dir L M Uni Panel Above Uni Pant Part Part	$Q (lbs) = M_{OT} (ft-lbs) = M_{OT} (ft-lbs) = f. W_D (plf) = f. W_D (plf) = Dist. 1 (ft.) = Dist. 2 (ft.) = Dist. 3 (ft.) = . W_{D1} (plf) = . W_{D2} (plf) = . W_{D2} (plf) = . W_{D3} (plf) =$								
(RH	$P_{D2}$ (lbs) = $P_{D3}$ (lbs) =								
Dir. R Dir. L Dir. R M Dir. L M LH end	$M_{R} (ft-lbs) =$ $M_{R} (ft-lbs) =$ $M_{R} (ft-lbs) =$ $M_{RT} (ft-lbs) =$ $M_{RT} (ft-lbs) =$ $M_{RT} (ft-lbs) =$ $M_{RT} (ft-lbs) =$	0 0							
LH e	nd Holdown :	0							
			1		1			1	
LH end RH end 1/2 in. c 0.138 in. c (At L <sub>EFF</sub> ) 1	Studs/Post : Studs/Post : <u>Shear T</u> dia. a.b. o/c = dia. shotpin = 6d toenails =	ransfer		2 x 6 Simps Simpson A3	Directly or blocking o/c = on LTP4 o/c = 35, A35F o/c =	ver shear wall	At L <sub>EFF</sub> =		]
	]								

0.00									
0			MU		SHEARWA	LL ANALYS	SIS	Sheet: L	<u>.</u>
			Elev. Floor?		L <sub>TOT</sub> =	RWALL ANALYSIS           L <sub>TOT</sub> = 0.0 ft.         q = 1           L' <sub>TOT</sub> = 0.0 ft.         q' = 1			
Load Ty	pe (W, EQ):		(L, R, Both)?	Both	L' <sub>TOT</sub> =	0.0 ft.	q' =	0. plf	
Ht. ( ft.) =									
	L(ft.) =								
APA TR157	H(II.) =								
Perforated	Length* =								
Shearwall	F =								
Allo									
Seleci	t Shearwall :								
	L								. <u>.</u>
Panel Ma	ark (above) :								
	q (above) =	0	0	0	0	0	0	0	0
H (a Panel Ab	above - ft.) =	0	0	0	0	0	0	0	0
Offset - fro	m LH end =	0	Ū	Ū	Ū	Ū	0	Ū	Ū
Dir R M Dir L M Unif Panel Above Unif [	$\begin{array}{l} Q (lbs) = \\ _{OT} (ft-lbs) = \\ _{OT} (ft-lbs) = \\ . W_D (plf) = \\ . W_D (plf) = \\ . Dist. 1 (ft.) = \end{array}$								
[ Part. Part. Part. (LH) (RH)	$\begin{array}{l} \text{Dist. 2 (ft.) =} \\ \text{Dist. 3 (ft.) =} \\ \text{W}_{\text{D1}} (\text{plf}) = \\ \text{W}_{\text{D2}} (\text{plf}) = \\ \text{W}_{\text{D3}} (\text{plf}) = \\ \text{P}_{\text{D1}} (\text{lbs}) = \\ \text{P}_{\text{D2}} (\text{lbs}) = \\ \text{P}_{\text{D3}} (\text{lbs}) = \\ \text{P}_{\text{D4}} (\text{lbs}) = \end{array}$								
Dir. R N Dir. L N	$\Lambda_{\rm R}$ (ft-lbs) =								
Dir. R M <sub>N</sub>	$r_{R}$ (ft-lbs) =	0							
Dir. L M <sub>N</sub>	<sub>ET</sub> (ft-lbs) =	0							
LH end L	Jplift ( lbs ) =	0							
RH end L	- ( adi ) πιια	0							
LH en	d Holdown :								
RH en	d Holdown :								
LH end RH end 1/2 in. d 0.138 in. d (At L <sub>EFF</sub> ) 16	Studs/Post : Studs/Post : <u>Shear T</u> ia. a.b. o/c = ia. shotpin = 6d toenails =	ransfer		2 x 6 Simps Simpson A3	Directly ov blocking o/c = on LTP4 o/c = 35, A35F o/c =	ver shear wall	At L <sub>EFF</sub> =		]

0.00									
0 MULTIPANEL SHEARWALL ANALYSIS Sheet: L									
		Elev. Floor?		L <sub>TOT</sub> = 0.0 ft.		g = <b>0</b> . plf			
Load 1	ype (W, EQ):		(L, R, Both)?	Both	L' <sub>TOT</sub> =	0.0 ft.	q' =	0. plf	
Ht. ( ft.) =									
	L ( ft.) =								
	H ( ft.) =								
APA TR157	Area* =								
Perforated	Lengtn <sup>*</sup> =								
Shearwaii	Η/L =								
AI	lowed Types :								
Sele	ct Shearwall:								
	r								
Panel Mark (above) :		0	0	0	0	0	0	0	
q (above) =		0	0	0	0	0	0	0	0
Panel Above L ( ft.) =		0	0	0	0	0	0	0	0
Offset - from LH end =									
Dir R I Dir L I Vr Panel Above Ur Par Par Par Par	$Q (lbs) = M_{OT} (ft-lbs) = M_{OT} (ft-lbs) =$ $M_{OT} (ft-lbs) =$ $M_{D} (plf) =$ Dist. 1 (ft.) = Dist. 2 (ft.) = Dist. 3 (ft.) = $t. W_{D1} (plf) =$ $t. W_{D2} (plf) =$ $t. W_{D3} (plf) =$								
(Lł	H) $P_{D1}$ (lbs) = $P_{D2}$ (lbs) = $P_{D3}$ (lbs) = H) $P_{D4}$ (lbs) =								
Dir. R Dir. L Dir. R M Dir. L M LH end RH end	$\begin{split} M_{R} & (\text{ ft-lbs }) = \\ M_{R} & (\text{ ft-lbs }) = \\ M_{NET} & (\text{ ft-lbs }) = \\ M_{NET} & (\text{ ft-lbs }) = \\ Uplift & (\text{ lbs }) = \\ Uplift & (\text{ lbs }) = \end{split}$	0 0 0 0							
LH e RH e	end Holdown : end Holdown :								
LH end RH end 1/2 in. 0.138 in. (At L <sub>EFF</sub> )	d Studs/Post : d Studs/Post : <u>Shear T</u> dia. a.b. o/c = dia. shotpin = 16d toenails =	ransfer		2 x 6 Simps Simpson A3	Directly ov blocking o/c = on LTP4 o/c = 35, A35F o/c =	ver shear wall	At L <sub>EFF</sub> =	[	]

0.00									
0 MULTIPANEL SHEARWALL ANALYSIS Sheet: L									
		Elev. Floor?		L <sub>TOT</sub> = 0.0 ft.		g = <b>0</b> . plf			
Load 1	ype (W, EQ):		(L, R, Both)?	Both	L' <sub>TOT</sub> =	0.0 ft.	q' =	0. plf	
Ht. ( ft.) =									1
	L ( ft.) =								
	H ( ft.) =								
APA TR157	Area* =								
Perforated	Lengtn <sup>*</sup> =								
Shearwaii	Η/L =								
AI	lowed Types :								
Sele	ct Shearwall:								
	r								
Panel Mark (above) :		0	0	0	0	0	0	0	
q (above) =		0	0	0	0	0	0	0	0
Panel Above L ( ft.) =		0	0	0	0	0	0	0	0
Offset - from LH end =									
Dir R I Dir L I Vr Panel Above Ur Par Par Par Par	$Q (lbs) =$ $M_{OT} (ft-lbs) =$ $M_{OT} (ft-lbs) =$ $M_{DT} (ft-lbs) =$ $M_{DT} (plf) =$ $Dist. 1 (ft.) =$ $Dist. 2 (ft.) =$ $Dist. 3 (ft.) =$ $t. W_{D1} (plf) =$ $t. W_{D2} (plf) =$ $t. W_{D3} (plf) =$								
(Lł	H) $P_{D1}$ (lbs) = $P_{D2}$ (lbs) = $P_{D3}$ (lbs) = H) $P_{D4}$ (lbs) =								
Dir. R Dir. L Dir. R M Dir. L M LH end RH end	$\begin{split} M_{R} & (\text{ ft-lbs }) = \\ M_{R} & (\text{ ft-lbs }) = \\ M_{NET} & (\text{ ft-lbs }) = \\ M_{NET} & (\text{ ft-lbs }) = \\ Uplift & (\text{ lbs }) = \\ Uplift & (\text{ lbs }) = \end{split}$	0 0 0 0							
LH e RH e	end Holdown : end Holdown :								
LH end RH end 1/2 in. 0.138 in. (At L <sub>EFF</sub> )	d Studs/Post : d Studs/Post : <u>Shear T</u> dia. a.b. o/c = dia. shotpin = 16d toenails =	ransfer		2 x 6 Simps Simpson A3	Directly ov blocking o/c = on LTP4 o/c = 35, A35F o/c =	ver shear wall	At L <sub>EFF</sub> =	[	]