

Stemwall Cont. Footing Calculator

Check continuous footings at highest (vertically) loaded section of wall excluding point loads.
From previous sections and by inspection the most critically loaded wall is at Wall Line 2

(plf)	Dead Load	Floor Live	Roof Live	0.6(Wind)
Roof	426	0	481	0
Wall	108	0	0	0
Floor	7	27	0	0
Stemwall	150	0	0	0
Wind	0	0	0	40
Totals	690	27	481	40

Roof LL or S =	20.9 psf
Roof DL =	18.5 psf
Roof Trib. Width =	23.0 ft
Wall DL =	12 psf
Wall Hgt. =	9 ft
Floor LL =	40.0 psf
Floor DL =	10.0 psf
Floor Trib. Width =	0.7 ft
Wind (ASD) =	40.0 plf

ASD Load Cases from ASCE 7-10:

- 2.) D + L = 717 plf
- 3.) D + (Lr or S) = 1,171 plf (governs)
- 6a.) D + .75L + .75(.6W) + .75(Lr or S) = 1,101 plf

Bearing Calculations:

Applied Bearing Pressure	Q _{asd} =	1,171 psf	
Eff. Allowable SBP	Q _e =	1,350 psf	
Footing Width Required	W _{req} =	10.4 in	
Footing Width	W _{footing} =	12 in	→ OK

p _{conc} =	150 pc
Steel Yield Strength =	60,000 psi
Conc. Comp. Strength =	3,000 psi
Soil Bearing Pressure =	1,500 psf
Reinf. Cover =	3 in
Reinf. Bar Size =	4
Soil Depth Above Ftg. =	18 in
p _{soil} =	100 pc
Stem Width =	6 in
Stem Hgt. =	24 in
Footing Width =	12 in
Footing Depth =	6 in

Strength Design Load Cases from ASCE 7-10:

- 1.) 1.4D = 966 plf
- 2.) 1.2D + 1.6L + .5(Lr or S) = 1,111 plf
- 3.) 1.2D + 1.6(Lr or S) + L = 1,624 plf (governs)
- 4.) 1.2D + 1.0W + L + .5(Lr or S) = 1,162 plf

Beam Shear Calculations (One Way Shear):

Ult. Applied Bearing Pressure	Q _u =	1,624 psf	
Applied Beam Shear	V _u =	101 lbs	
Allowable Beam Shear	V _c =	2,218 lbs (ACI 11-3)	
Footing Depth Required	D _{req} =	0.3 in	
Footing Depth	D _{footing} =	6.0 in	→ OK

Beam Shear Calculations (One Way Shear):

<u>Unreinforced Concrete</u>	
V _u =	406 lbs
V _c =	2,103 lbs (ACI 22-9)
D _{req} =	1.2 in
D _{footing} =	6.0 in → OK

Bending Calculations:

	a =	0.26 in	
Cantilever length	L _{cant} =	3.0 in	
Factored Bending Moment	M _u =	609 in-lb	
Moment Strength	M _n =	14,997 in-lb	

Bending Calculations:

<u>Unreinforced Concrete</u>	
S =	32.0 in ³
M _u =	609 in-lb
M _n =	5,258 in-lb (ACI 22-2)
D _{req} =	0.7 in
D _{footing} =	6.0 in → OK

Transverse Reinforcement Calculations:

Mu/φbd ²	R _n =	11.1 psi	
Steel Ratio	ρ =	0.0002	
Steel Req. based on Moment	A _{s(1)} =	0.005 in ²	
Steel Req. based on Shrink	A _{s(2)} =	0.130 in ² (ACI 7.12)	
Controlling Reinf. Steel	A _{s(req)} =	0.130 in ²	
Required Spacing with #4 bars =		18.18 in o/c	
Selected Transverse Spacing:	#4 bars @	18 in o/c	
Reinforcement Area Provided	A _s =	0.131 in ² → OK	

Eff. Depth to Top Layer of Steel

d =	2.25 in
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(Transverse Reinforcement Unnecessary)

Development Length Calculations:

spacing/cover dimension	c =	3.0 in	
Transverse Reinf. Factor	c + K _{tr} /d _b =	6 (use 2.5)	
Length Req.	L _d =	13.0 in (ACI 12-1)	
Length Available	L _{d-sup} =	0 in	

Note: Plain concrete adequate for bending, therefore development length not required.

λ =	1.0 (lightweight aggregate factor)
ψ _t =	1.0 (reinforcement location factor)
ψ _e =	1.0 (coating factor)
ψ _s =	0.8 (reinforcement size factor)
K _{tr} =	0.0 (transverse reinf. Index)

Longitudinal Reinforcement Calculations:

Steel Req. based on Shrink	A _{s(2)} =	0.130 in ² (ACI 7.12)	
Controlling Reinf. Steel	A _{s(req)} =	0.130 in ²	
Required number of #4 bars =		0.66	
Selected Longitudinal Bars:		2 - Cont. #4 bars	
Reinforcement Area Provided	A _s =	0.393 in ² → OK	